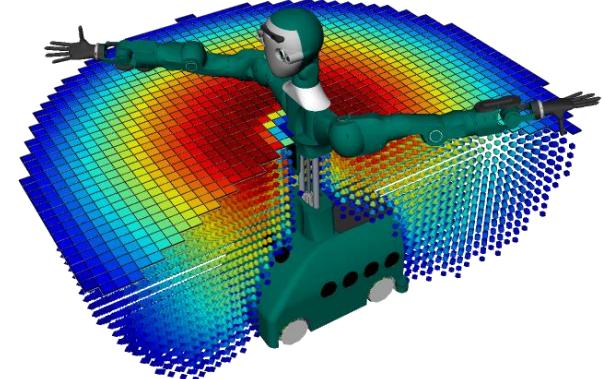
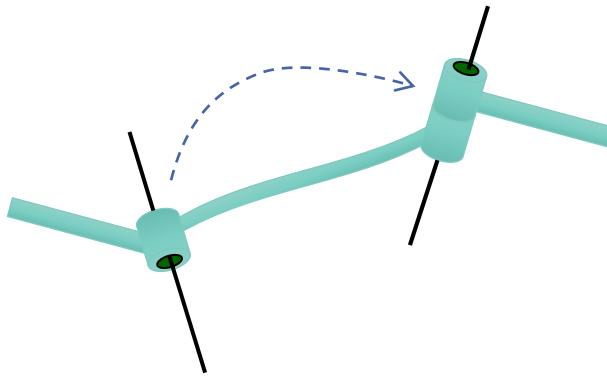


Robotics I: Introduction to Robotics

Exercise 2: Kinematics

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<https://www.humanoids.kit.edu>



Task 6 & 7 From Exercise 01

- Brief summary
(see slides of previous exercise for full version)

Exercise 6: Quaternions

Show that the space of unit quaternions S^3 is a subgroup of the quaternions \mathbb{H} .

Remark: G is a group (G, \cdot) if and only if:

1. Closed w.r.t. (\cdot) : $\forall a, b \in G : a \cdot b \in G$
2. Associativity: $\forall a, b, c \in G : (a \cdot b) \cdot c = a \cdot (b \cdot c)$
3. Identity element: $\exists e \in G : \forall a \in G : e \cdot a = a \cdot e = a$
4. Inverse element: $\forall a \in G : \exists a^{-1} : a \cdot a^{-1} = e$

Exercise 6.1: Closure (Tricky)

1. Closed w.r.t. (\cdot): $\forall a, b \in G : a \cdot b \in G$

$$\forall \mathbf{a}, \mathbf{b} \in S^3 : \mathbf{a} \cdot \mathbf{b} \in S^3$$

$$\|\mathbf{a} \cdot \mathbf{b}\|^2 =$$

Exercise 6.1: Closure (Tricky)

- Closed w.r.t. (\cdot): $\forall a, b \in G : a \cdot b \in G$

$$\forall \mathbf{a}, \mathbf{b} \in S^3 : \mathbf{a} \cdot \mathbf{b} \in S^3$$

$$\|\mathbf{a} \cdot \mathbf{b}\|^2 = \|(a_0, a_1, a_2, a_3) \cdot (b_0, b_1, b_2, b_3)\|^2$$

$$\begin{aligned}
 &= a_3^2 b_3^2 + a_2^2 b_3^2 + a_1^2 b_3^2 + a_0^2 b_3^2 \\
 &+ a_3^2 b_2^2 + a_2^2 b_2^2 + a_1^2 b_2^2 + a_0^2 b_2^2 \\
 &+ a_3^2 b_1^2 + a_2^2 b_1^2 + a_1^2 b_1^2 + a_0^2 b_1^2 \\
 &+ a_3^2 b_0^2 + a_2^2 b_0^2 + a_1^2 b_0^2 + a_0^2 b_0^2
 \end{aligned}$$

Exercise 6.1: Closure (Tricky)

1. Closed w.r.t. (\cdot): $\forall a, b \in G : a \cdot b \in G$

$$\forall \mathbf{a}, \mathbf{b} \in S^3 : \mathbf{a} \cdot \mathbf{b} \in S^3$$

$$\begin{aligned}\|\mathbf{a} \cdot \mathbf{b}\|^2 &= \|(a_0, a_1, a_2, a_3) \cdot (b_0, b_1, b_2, b_3)\|^2 \\&= b_3^2 \cdot \|\mathbf{a}\|^2 + b_2^2 \cdot \|\mathbf{a}\|^2 + b_1^2 \cdot \|\mathbf{a}\|^2 + b_0^2 \cdot \|\mathbf{a}\|^2 \\&= (b_3^2 + b_2^2 + b_1^2 + b_0^2) \cdot \|\mathbf{a}\|^2 \\&= \|\mathbf{b}\|^2 \cdot \|\mathbf{a}\|^2 = 1 \cdot 1 = 1\end{aligned}$$

Exercise 6.2 & 6.3: Associativity and Identity Element

2. Associativity: $\forall a, b, c \in G : (a \cdot b) \cdot c = a \cdot (b \cdot c)$

3. Identity element: $\exists e \in G : \forall a \in G : e \cdot a = a \cdot e = a$

Exercise 6.2 & 6.3: Associativity and Identity Element

2. Associativity: $\forall a, b, c \in G : (a \cdot b) \cdot c = a \cdot (b \cdot c)$

Unit quaternions are a subset of quaternions. Multiplications of quaternions are associative.

3. Identity element: $\exists e \in G : \forall a \in G : e \cdot a = a \cdot e = a$

The identity element is $e = (1, 0, 0, 0)$.

Exercise 6.4: Inverse Element

4. Inverse element: $\forall a \in G : \exists a^{-1} : a \cdot a^{-1} = e$

$$q \in S^3 \Rightarrow q^{-1} \in S^3$$

Exercise 6.4: Inverse Element

4. Inverse element: $\forall a \in G : \exists a^{-1} : a \cdot a^{-1} = e$

$$q \in S^3 \Rightarrow q^{-1} \in S^3$$

$$\|q^{-1}\|^2 = \left\| \frac{q^*}{\|q\|^2} \right\|^2$$

$$= \left\| \frac{q^*}{1} \right\|^2$$

$$= 1$$

Exercise 7: Rotations and Machine Learning

Rotations as input and output of learned models

1. Compare the **representations of rotations** as

- Euler angles,
- Quaternions, and
- Rotation matrices

with respect to how suitable they are as the **output** of a machine learning approach (e.g., neural networks)

2. A neural network, which has been trained to output rotation matrices, yields the matrix A :

$$A = \begin{pmatrix} 0.6 & 0.1 & 0.1 \\ 0.5 & 0.9 & 0.5 \\ 0.1 & 0.0 & 0.7 \end{pmatrix}$$

Determine a rotation matrix R that is as “close” to A as possible.

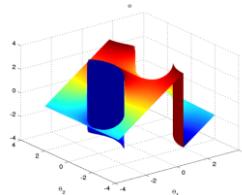
Exercise 7.1: Euler Angles and ML

Euler angles: $\alpha, \beta, \gamma \in [0, 2\pi]$

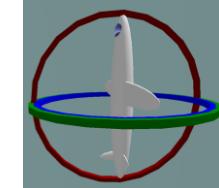
Rotation around three axes (several conventions)

- + Minimal representation for 3 Degree of Freedom
- + All values are valid, even beyond the intervall $[0, 2\pi]$

- Not continuous



- Multi-coverage
A rotation can be described by multiple tuples α, β, γ
(e.g., Gimbal lock)



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Exercise 7.1: Quaternions and ML

$$S^3 = \{ \mathbf{q} \in \mathbb{H} \mid \|\mathbf{q}\|^2 = 1 \}$$

$$\mathbf{q} = \left(\cos \frac{\Phi}{2}, \quad \mathbf{a} \cdot \sin \frac{\Phi}{2} \right)$$

- + Easy to normalize $\mathbf{p} \in \mathbb{H}, \mathbf{p} \notin S^3: \quad \mathbf{q} = \frac{\mathbf{p}}{\|\mathbf{p}\|} \in S^3$
- + Local interpolation is linear:

$$\text{SLERP}(\mathbf{q}_1, \mathbf{q}_2, t) = \frac{\sin((1-t)\theta)}{\sin\theta} \cdot \mathbf{q}_1 + \frac{\sin t\theta}{\sin\theta} \cdot \mathbf{q}_2$$

- Representation is not minimal: 1 redundant value ($\|\mathbf{q}\|^2 = 1$)
- Double coverage: Each rotation can be described by two different unit quaternions

Exercise 7.1: Rotation Matrices and ML

$$R_{z,\alpha} = \begin{pmatrix} \cos \alpha & -\sin \alpha & 0 \\ \sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

- + Single coverage:
A rotation corresponds to exactly one rotation matrix
- + Local interpolation is linear: $\sin \alpha \approx \alpha$, $\cos \alpha \approx 1$, for very small α
- Normalization is possible, but complex
→ Gram-Schmidt, QR decomposition, SVD
- Highly redundant representation: 6 redundant values

Exercise 7.2: Rotation Matrices and ML

A neural network, which has been trained to output rotation matrices, yields the matrix A :

$$A = \begin{pmatrix} 0.6 & 0.1 & 0.1 \\ 0.5 & 0.9 & 0.5 \\ 0.1 & 0.0 & 0.7 \end{pmatrix}$$

Determine a rotation matrix R that is as “close” to A as possible.

Exercise 7.2: Gram-Schmidt Orthogonalization

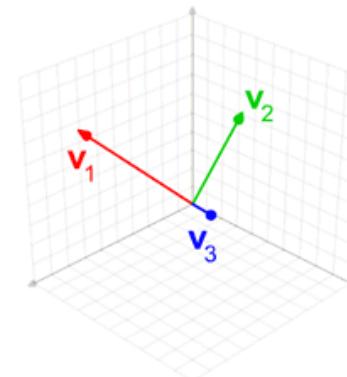
- Orthogonalization
 - Given: Linearly independent vectors w_1, \dots, w_3
 - Unknown: Pairwise orthogonal vectors v_1, \dots, v_3 that span the same subspace
- Gram-Schmidt

- $v_1 = w_1$

- $v_2 = w_2 - \frac{v_1 \cdot w_2}{v_1 \cdot v_1} \cdot v_1$

- $v_3 = w_3 - \frac{v_1 \cdot w_3}{v_1 \cdot v_1} \cdot v_1 - \frac{v_2 \cdot w_3}{v_2 \cdot v_2} \cdot v_2$

- Projection on previous vectors
- Subtract the projected part



Exercise 7.2: Gram-Schmidt Orthogonalization

■ Orthogonalization

- Given: Linearly independent vectors w_1, \dots, w_3
- Unknown: Pairwise orthogonal vectors v_1, \dots, v_3 that span the same subspace

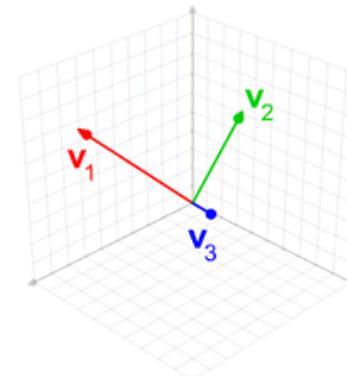
■ Gram-Schmidt

$$v_1 = w_1 = \begin{pmatrix} 0.6 \\ 0.5 \\ 0.1 \end{pmatrix}$$

$$v_2 = w_2 - \frac{v_1 \cdot w_2}{v_1 \cdot v_1} \cdot v_1 \approx \begin{pmatrix} -0.394 \\ 0.489 \\ -0.082 \end{pmatrix}$$

$$v_3 = w_3 - \frac{v_1 \cdot w_3}{v_1 \cdot v_1} \cdot v_1 - \frac{v_2 \cdot w_3}{v_2 \cdot v_2} \cdot v_2 \approx \begin{pmatrix} -0.122 \\ 0.013 \\ 0.669 \end{pmatrix}$$

- Projection on previous vectors
- Subtract the projected part



Exercise 7.2: Normalization

Normalization:

$$e_1 = \frac{v_1}{\|v_1\|} \approx \frac{1}{\sqrt{0.62}} \cdot \begin{pmatrix} 0.6 \\ 0.5 \\ 0.1 \end{pmatrix} \approx \begin{pmatrix} 0.762 \\ 0.635 \\ 0.127 \end{pmatrix}$$

$$e_2 = \frac{v_2}{\|v_2\|} \approx \frac{1}{\sqrt{0.401}} \cdot \begin{pmatrix} -0.394 \\ 0.489 \\ -0.082 \end{pmatrix} \approx \begin{pmatrix} -0.622 \\ 0.772 \\ -0.129 \end{pmatrix}$$

$$e_3 = \frac{v_3}{\|v_3\|} \approx \frac{1}{\sqrt{0.463}} \cdot \begin{pmatrix} -0.122 \\ 0.013 \\ 0.669 \end{pmatrix} \approx \begin{pmatrix} -0.179 \\ 0.019 \\ 0.984 \end{pmatrix}$$

Exercise 7.2: Result

■ Input:

$$A = \begin{pmatrix} 0.6 & 0.1 & 0.1 \\ 0.5 & 0.9 & 0.5 \\ 0.1 & 0.0 & 0.7 \end{pmatrix}$$

■ Orthonormal basis vectors:

$$e_1 = \begin{pmatrix} 0.762 \\ 0.635 \\ 0.127 \end{pmatrix}, e_2 = \begin{pmatrix} -0.622 \\ 0.772 \\ -0.129 \end{pmatrix}, e_3 = \begin{pmatrix} -0.179 \\ 0.019 \\ 0.984 \end{pmatrix}$$

■ Rotation matrix:

$$R = \begin{pmatrix} 0.762 & -0.622 & -0.179 \\ 0.635 & 0.772 & 0.019 \\ 0.127 & -0.129 & 0.984 \end{pmatrix}$$

Python for Next Exercises

- Install python (≥ 3.6) and an IDE
 - E.g., PyCharm Community Edition (Linux/Windows/macOS)
<https://www.jetbrains.com/pycharm/download#community-edition>

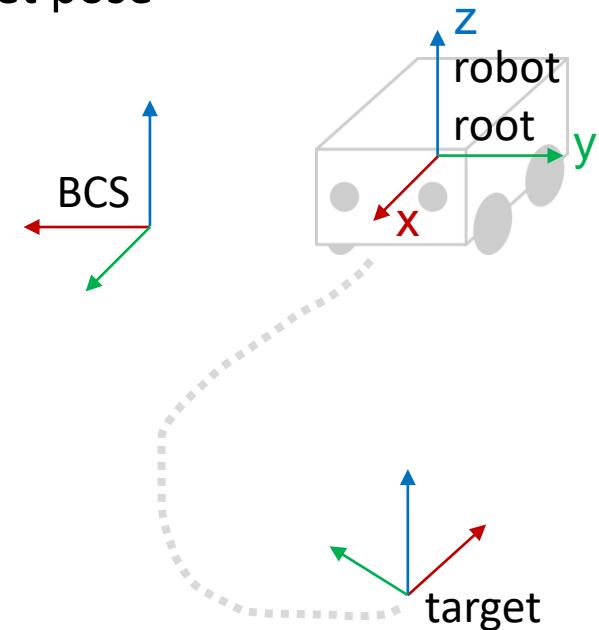
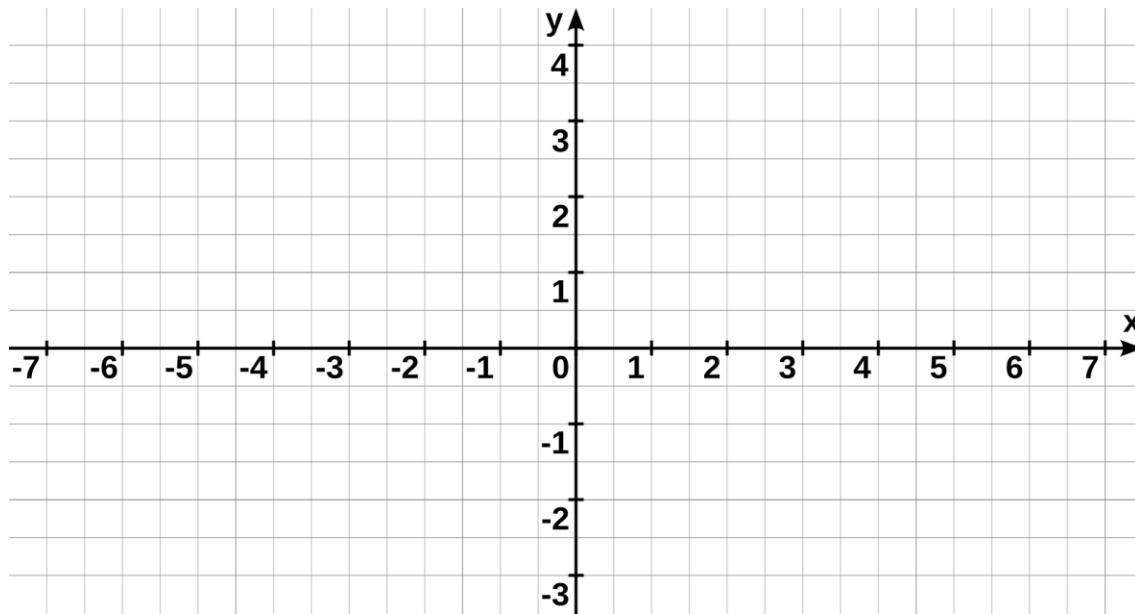
- Robotics Toolbox (Peter Corke)
 - <https://github.com/petercorke/robotics-toolbox-python>
 - Install via git repository or, recommended, via PyPI:
`pip3 install roboticstoolbox-python [collision]`

- Give it a try: Solve exercise sheet 1 in python



Exercise 1: Transformations

- Robot with root pose, basis coordinate system, target pose



Exercise 1.1: Interpretation of a Pose

- Let the initial root pose of a robot, described in the BCS, be given as

$${}^{BCS}T_{root} = \begin{pmatrix} \frac{1}{2}\sqrt{3} & -\frac{1}{2} & 0 & 3 \\ \frac{1}{2} & \frac{1}{2}\sqrt{3} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

- Which transformation does ${}^{BCS}T_{root}$ describe?
- At which position is the robot's root located?
Draw the position in the BCS.

Exercise 1.1 (i): Interpretation of a Pose

$${}^{BCS}T_{root} = \begin{pmatrix} \frac{1}{2}\sqrt{3} & -\frac{1}{2} & 0 & 3 \\ \frac{1}{2} & \frac{1}{2}\sqrt{3} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

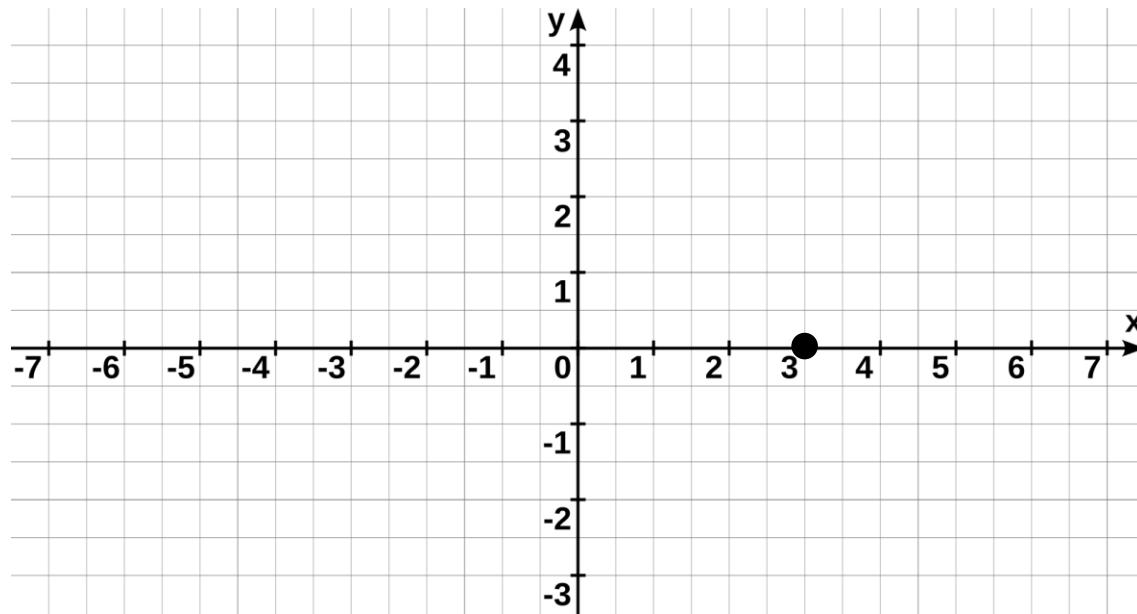
Transformation described by ${}^{BCS}T_{root}$:

- Translation by 3 along x-axis
- Rotation around z-axis, by 30°

α	0°	30°	60°	90°
$\sin(\alpha)$	0	$\frac{1}{2}$	$\frac{\sqrt{3}}{2}$	1
$\cos(\alpha)$	1	$\frac{\sqrt{3}}{2}$	$\frac{1}{2}$	0

Exercise 1.1 (ii): Interpretation of a Pose

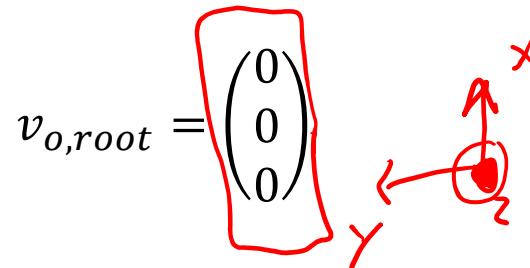
- Robot position: $(3, 0, 0)^\top$



Exercise 1.1 (iv): Interpretation of a Pose

- Vectors (in the robot's root coordinate system):

$$v_{x,root} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}, \quad v_{y,root} = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}, \quad v_{z,root} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$



Exercise 1.1 (iv): Interpretation of a Pose

- Vectors (in the robot's root coordinate system):

$$v_{x,root} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}, \quad v_{y,root} = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}, \quad v_{z,root} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}, \quad v_{o,root} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

- Vectors (in the BCS):

$$v_{BCS} = {}^{BCS}T_{root} \cdot v_{root}$$

Exercise 1.1 (iv): Interpretation of a Pose

- Vectors (in the robot's root coordinate system):

$$v_{x,root} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}, \quad v_{y,root} = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}, \quad v_{z,root} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}, \quad v_{o,root} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

- Vectors (in the BCS):

$$v_{BCS} = {}^{BCS}T_{root} \cdot v_{root}$$

$$\begin{pmatrix} \frac{1}{2}\sqrt{3} & -\frac{1}{2} & 0 & 3 \\ \frac{1}{2} & \frac{1}{2}\sqrt{3} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 1 \\ 0 \\ 0 \\ 1 \end{pmatrix} = \begin{pmatrix} 3 + \frac{1}{2}\sqrt{3} \\ \frac{1}{2} \\ 0 \\ 1 \end{pmatrix} \Rightarrow v_{x,BCS} = \begin{pmatrix} 3 + \frac{1}{2}\sqrt{3} \\ \frac{1}{2} \\ 0 \end{pmatrix} \quad \text{etc.}$$

Exercise 1.1 (iv): Interpretation of a Pose

- Vectors (in the robot's root coordinate system):

$$v_{x,root} = \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix}, \quad v_{y,root} = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}, \quad v_{z,root} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}, \quad v_{o,root} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

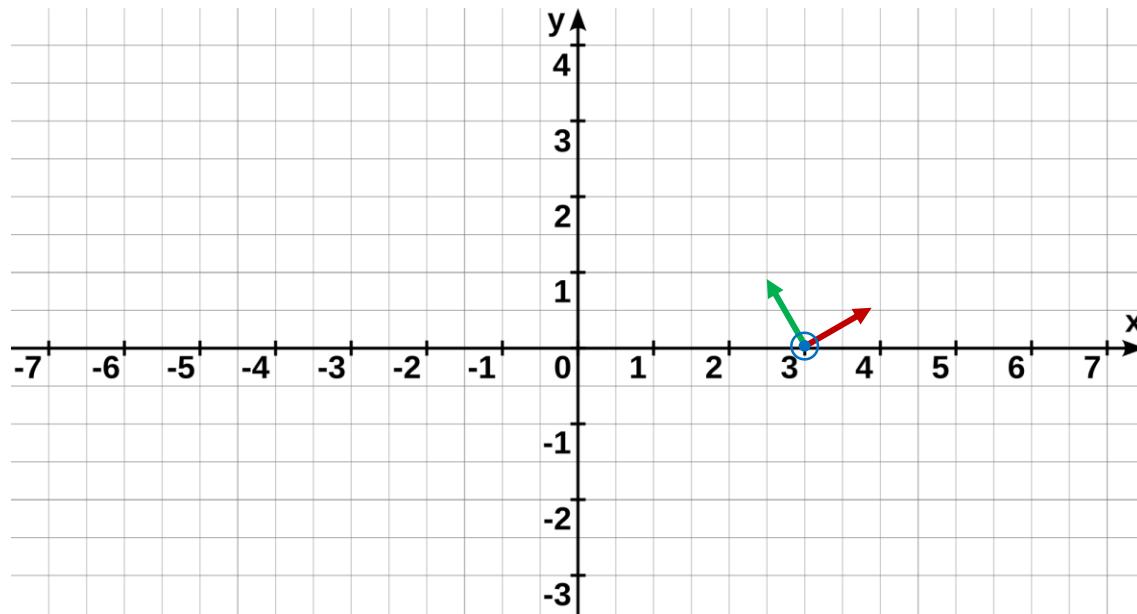
- Vectors (in the BCS):

$$v_{BCS} = {}^{BCS}T_{root} \cdot v_{root}$$

$$v_{x,BCS} = \begin{pmatrix} 3 + \frac{1}{2}\sqrt{3} \\ \frac{1}{2} \\ 0 \end{pmatrix}, \quad v_{y,BCS} = \begin{pmatrix} \frac{5}{2} \\ \frac{1}{2}\sqrt{3} \\ 0 \end{pmatrix}, \quad v_{z,BCS} = \begin{pmatrix} 3 \\ 0 \\ 1 \end{pmatrix}, \quad v_{o,BCS} = \begin{pmatrix} 3 \\ 0 \\ 0 \end{pmatrix}$$

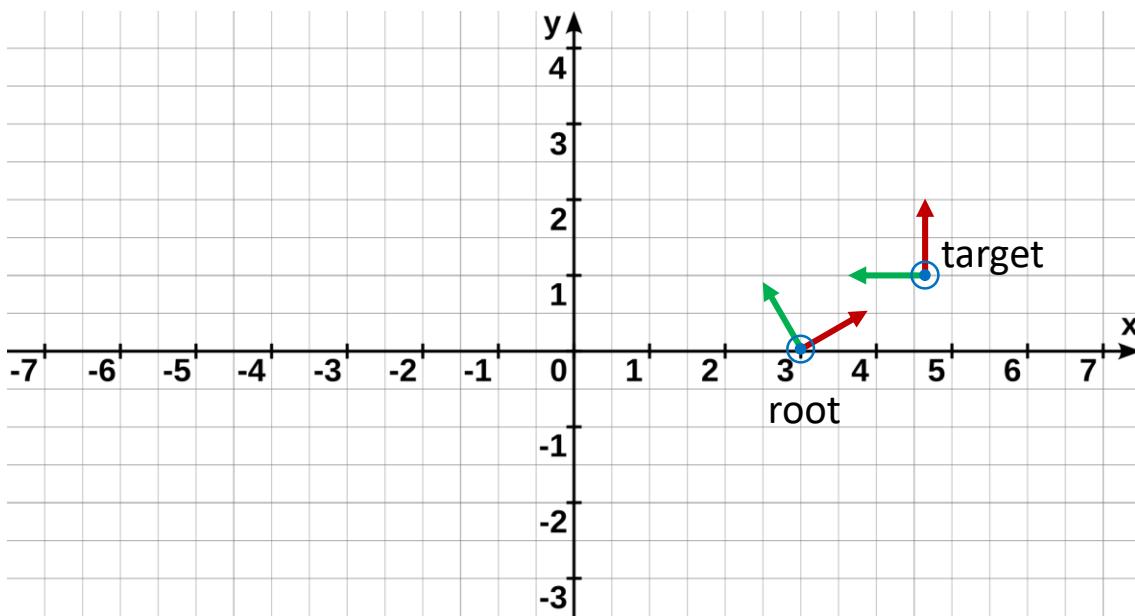
Exercise 1.1 (iv): Interpretation of a Pose

- Robot root pose ${}^{BCS}T_{root}$



Exercise 1.2 (i): Conversion Between Coordinate Systems

- Target pose ${}^{BCS}T_{target}$



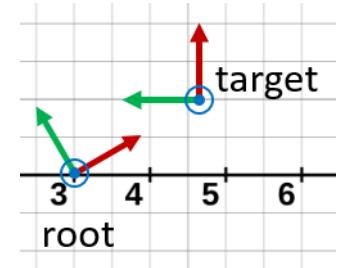
$${}^{BCS}T_{target} = \begin{pmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \\ 0 & 0 & 0 \end{pmatrix} \begin{pmatrix} 3 + \sqrt{3} \\ 1 \\ 0 \\ 1 \end{pmatrix}$$

x-axis of target:
in y-direction of BCS

$$\begin{pmatrix} 0 & -1 & 0 \\ 1 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} = \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix}$$

Exercise 1.2 (ii): Conversion Between Coordinate Systems

- Target pose in the robot's root coordinate system
 - Searched: ${}^{root}T_{target}$
 - Known relation: ${}^{BCS}T_{root} \cdot {}^{root}T_{target} = {}^{BCS}T_{target}$



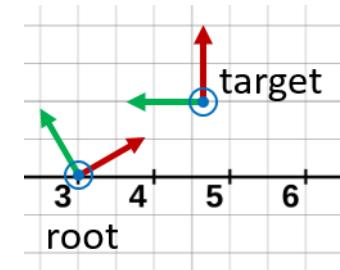
Exercise 1.2 (ii): Conversion Between Coordinate Systems

- Target pose in the robot's root coordinate system

- Searched: ${}^{root}T_{target}$

- Known relation: ${}^{BCS}T_{root} \cdot {}^{root}T_{target} = {}^{BCS}T_{target}$

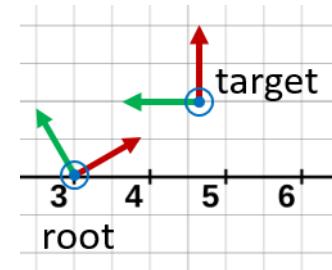
$$\Leftrightarrow {}^{root}T_{target} = \underline{\underline{({}^{BCS}T_{root})^{-1} \cdot {}^{BCS}T_{target}}}$$



Exercise 1.2 (ii): Conversion Between Coordinate Systems

Reminder: $\begin{pmatrix} R & \mathbf{t} \\ 0 & 1 \end{pmatrix}^{-1} = \begin{pmatrix} R^T & -R^T \mathbf{t} \\ 0 & 1 \end{pmatrix}$

$$\left({}^{BCS}T_{root} \right)^{-1} = \begin{pmatrix} \frac{1}{2}\sqrt{3} & -\frac{1}{2} & 0 & 3 \\ \frac{1}{2} & \frac{1}{2}\sqrt{3} & 0 & 0 \\ \frac{1}{2} & \frac{1}{2}\sqrt{3} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}^{-1} = \begin{pmatrix} \frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & -\frac{3}{2}\sqrt{3} \\ -\frac{1}{2} & \frac{1}{2}\sqrt{3} & 0 & \frac{3}{2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

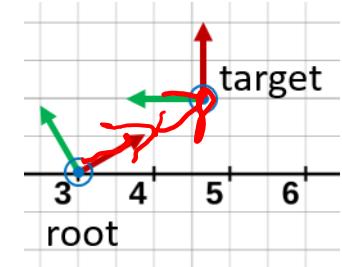


Exercise 1.2 (ii): Conversion Between Coordinate Systems

$${}^{root}T_{target} = ({}^{BCS}T_{root})^{-1} \cdot {}^{BCS}T_{target}$$

$$= \begin{pmatrix} \frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & -\frac{3}{2}\sqrt{3} \\ -\frac{1}{2} & \frac{1}{2}\sqrt{3} & 0 & \frac{3}{2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 0 & -1 & 0 & 3 + \sqrt{3} \\ 1 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$= \begin{pmatrix} \frac{1}{2} & -\frac{1}{2}\sqrt{3} & 0 & \frac{3}{2}\sqrt{3} + \frac{3}{2} + \frac{1}{2} - \frac{3}{2}\sqrt{3} \\ \frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & -\frac{3}{2} - \frac{1}{2}\sqrt{3} + \frac{1}{2}\sqrt{3} + \frac{3}{2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} \frac{1}{2} & -\frac{1}{2}\sqrt{3} & 0 & 2 \\ \frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

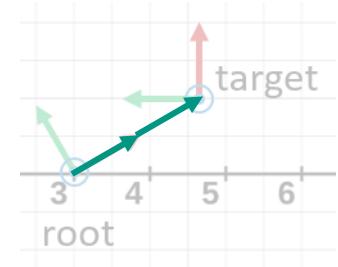


Exercise 1.2 (ii): Conversion Between Coordinate Systems

$${}^{root}T_{target} = ({}^{BCS}T_{root})^{-1} \cdot {}^{BCS}T_{target}$$

$$= \begin{pmatrix} \frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & -\frac{3}{2}\sqrt{3} \\ -\frac{1}{2} & \frac{1}{2}\sqrt{3} & 0 & \frac{3}{2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 0 & -1 & 0 & 3 + \sqrt{3} \\ 1 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$= \begin{pmatrix} \frac{1}{2} & -\frac{1}{2}\sqrt{3} & 0 & \frac{3}{2}\sqrt{3} + \frac{3}{2} + \frac{1}{2} - \frac{3}{2}\sqrt{3} \\ \frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & -\frac{3}{2} - \frac{1}{2}\sqrt{3} + \frac{1}{2}\sqrt{3} + \frac{3}{2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} = \begin{pmatrix} \frac{1}{2} & -\frac{1}{2}\sqrt{3} & 0 & 2 \\ \frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$



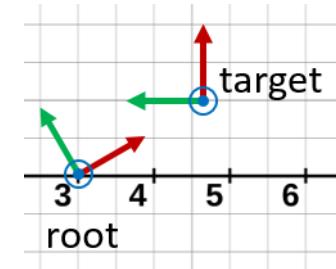
Exercise 1.2 (iii): Conversion Between Coordinate Systems

- Robot root pose in the target's coordinate system

- Searched: ${}^{target}T_{root}$

- Known relation: ${}^{BCS}T_{target} \cdot {}^{target}T_{root} = {}^{BCS}T_{root}$

$$\Leftrightarrow {}^{target}T_{root} = ({}^{BCS}T_{target})^{-1} \cdot {}^{BCS}T_{root}$$



Exercise 1.2 (iii): Conversion Between Coordinate Systems

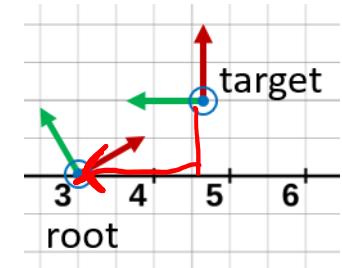
- Robot root pose in the target's coordinate system

- Searched: ${}^{target}T_{root}$

- Known relation: ${}^{BCS}T_{target} \cdot {}^{target}T_{root} = {}^{BCS}T_{root}$

$$\Leftrightarrow {}^{target}T_{root} = ({}^{BCS}T_{target})^{-1} \cdot {}^{BCS}T_{root}$$

$$= \dots = \begin{pmatrix} \frac{1}{2} & \frac{1}{2}\sqrt{3} & 0 & -1 \\ -\frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & \sqrt{3} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$



Small Exercise

- To calculate ${}^{root}T_{target}$, we used ${}^{BCS}T_{root} \cdot {}^{\underline{root}}T_{target} = {}^{BCS}T_{target}$ as a starting point.
 Could we alternatively have used ${}^{BCS}T_{target} \cdot {}^{\underline{target}}T_{root} = {}^{BCS}T_{root}$?

- Yes, ${}^{target}T_{root}$ and ${}^{root}T_{target}$ are the same.
- Yes, together with ${}^{root}T_{target} = ({}^{target}T_{root})^{-1}$.
- Yes, together with ${}^{root}T_{target} = ({}^{target}T_{root})^T$.
- No, these equations describe completely different situations.

Small Exercise

- To calculate ${}^{root}T_{target}$, we used ${}^{BCS}T_{root} \cdot {}^{root}T_{target} = {}^{BCS}T_{target}$ as a starting point.
Could we alternatively have used ${}^{BCS}T_{target} \cdot {}^{target}T_{root} = {}^{BCS}T_{root}$?
- a) Yes, ${}^{target}T_{root}$ and ${}^{root}T_{target}$ are the same.
- b) Yes, together with ${}^{root}T_{target} = ({}^{target}T_{root})^{-1}$.
- c) Yes, together with ${}^{root}T_{target} = ({}^{target}T_{root})^T$.
- d) No, these equations describe completely different situations.

Small Exercise

$$\begin{aligned}
 ({^{target}T_{root}})^{-1} &= \begin{pmatrix} \frac{1}{2} & \frac{1}{2}\sqrt{3} & 0 & -1 \\ -\frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & \sqrt{3} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}^{-1} = \begin{pmatrix} \frac{1}{2} & -\frac{1}{2}\sqrt{3} & 0 & \frac{1}{2} + \frac{3}{2} \\ \frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & \frac{1}{2}\sqrt{3} - \frac{1}{2}\sqrt{3} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \\
 &= \begin{pmatrix} \frac{1}{2} & -\frac{1}{2}\sqrt{3} & 0 & 2 \\ \frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} = {^root}T_{target} \text{ as previously calculated}
 \end{aligned}$$

Exercise 1.3 (i): Local and Global Transformation

- Transformation T corresponding to 60° rotation around z-axis:

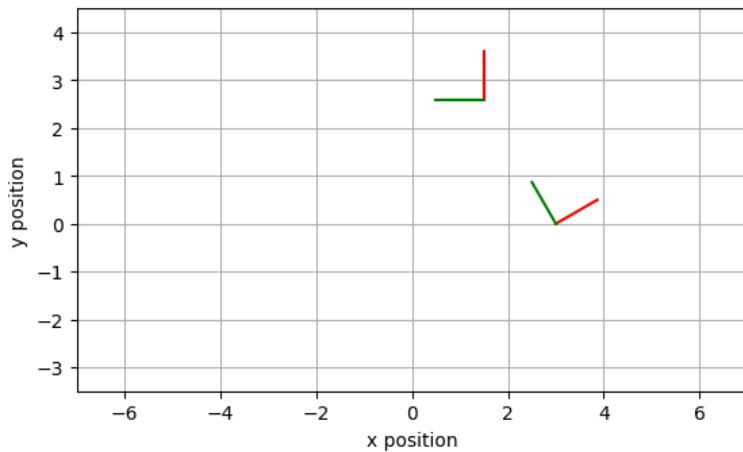
$$T = \begin{pmatrix} \frac{1}{2} & -\frac{1}{2}\sqrt{3} & 0 & 0 \\ \frac{1}{2}\sqrt{3} & \frac{1}{2} & 0 & 0 \\ 0 & 0 & 1 & 0 \\ \cdot & 0 & 0 & 1 \end{pmatrix}$$

α	0°	30°	60°	90°
$\sin(\alpha)$	0	$\frac{1}{2}$	$\frac{\sqrt{3}}{2}$	1
$\cos(\alpha)$	1	$\frac{\sqrt{3}}{2}$	$\frac{1}{2}$	0

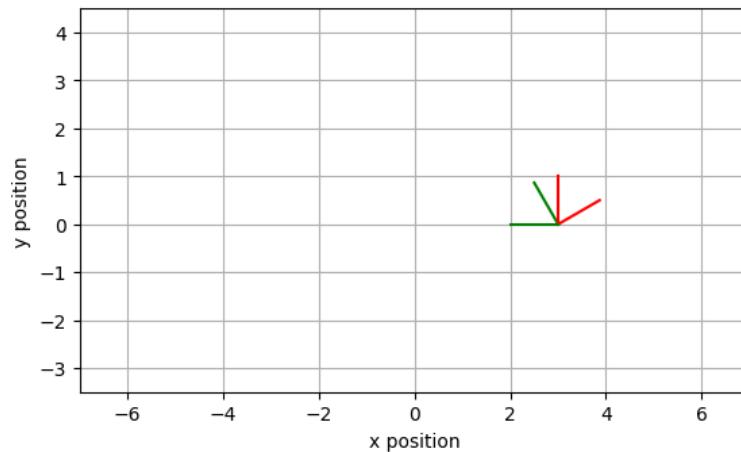
Exercise 1.3 (ii-iv): Local and Global Transformation

- Application from the left and from the right:

$$T \cdot {}^{BCS}T_{root}$$



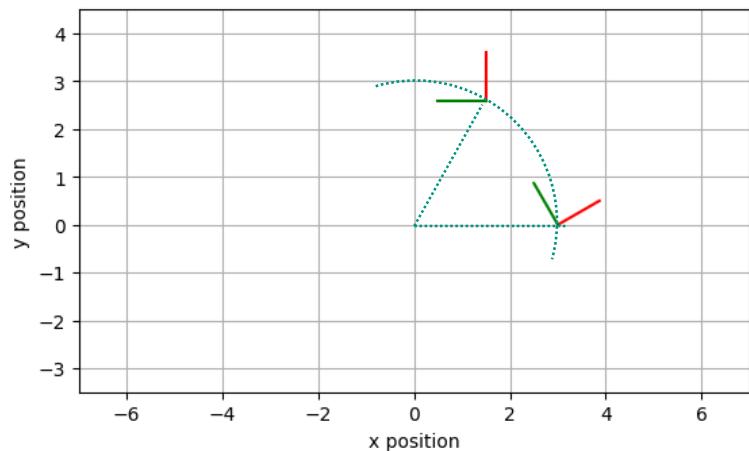
$${}^{BCS}T_{root} \cdot T$$



Exercise 1.3 (ii-iv): Local and Global Transformation

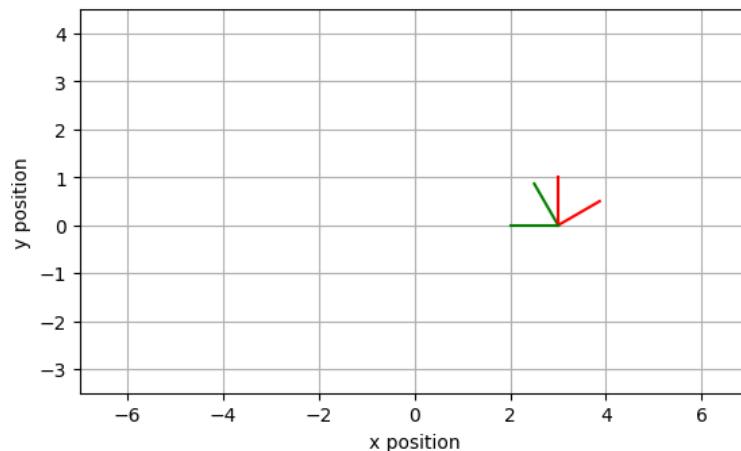
- Application from the left and from the right:

$$T \cdot {}^{BCS}T_{root}$$



Global transformation

$${}^{BCS}T_{root} \cdot T$$

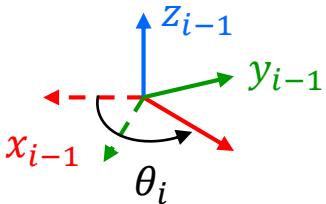


Local transformation

DH Transformation Matrices (1)

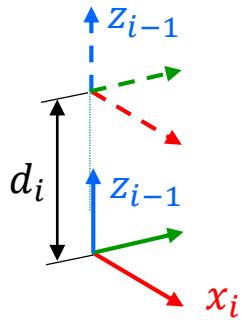
Transformation from LCS_{i-1} to LCS_i

1. A **rotation θ_i around the Z_{i-1} -axis** so that the x_{i-1} -axis is parallel to the x_i -axis.



$$R_{Z_{i-1}}(\theta_i) = \begin{pmatrix} \cos \theta_i & -\sin \theta_i & 0 & 0 \\ \sin \theta_i & \cos \theta_i & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

2. A **translation d_i along the Z_{i-1} -axis** to the point where Z_{i-1} and x_i intersect.



$$T_{Z_{i-1}}(d_i) = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_i \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

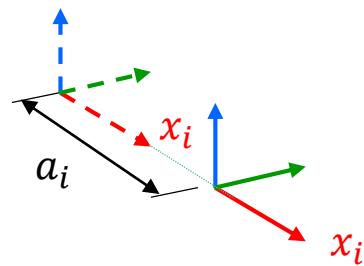
LCS_i : Local Coordinate System of joint i

DH Transformation Matrices (2)

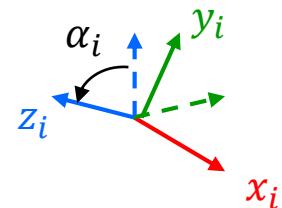
Transformation from LCS_{i-1} to LCS_i

3. A **translation** a_i along the x_i -axis to align the origins of the coordinate systems.

4. A **rotation** α_i around the x_i -axis to convert the z_{i-1} -axis into the z_i -axis.



$$T_{x_i}(a_i) = \begin{pmatrix} 1 & 0 & 0 & a_i \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$



$$R_{x_i}(\alpha_i) = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & \cos \alpha_i & -\sin \alpha_i & 0 \\ 0 & \sin \alpha_i & \cos \alpha_i & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

LCS_i : Local Coordinate System of joint i

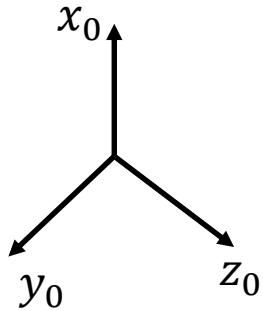
DH Transformation Matrices (3)

Transformation from LCS_{i-1} to LCS_i

$$\begin{aligned}
 A_{i-1,i} &= R_{z_{i-1}}(\theta_i) \cdot T_{z_{i-1}}(d_i) \cdot T_{x_i}(a_i) \cdot R_{x_i}(\alpha_i) \\
 &= \begin{bmatrix} \cos \theta_i & -\sin \theta_i \cdot \cos \alpha_i & \sin \theta_i \cdot \sin \alpha_i & a_i \cdot \cos \theta_i \\ \sin \theta_i & \cos \theta_i \cdot \cos \alpha_i & -\cos \theta_i \cdot \sin \alpha_i & a_i \cdot \sin \theta_i \\ 0 & \sin \alpha_i & \cos \alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}
 \end{aligned}$$

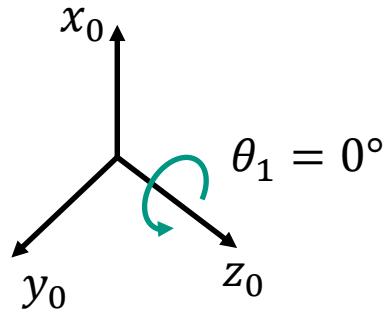
Exercise 2.1 (i): DH Transformation

- DH parameters: $\theta_1 = 0^\circ, d_1 = 60 \text{ mm}, a_1 = 0 \text{ mm}, \alpha_1 = 180^\circ$
- Rotation around z_0 -axis by $\theta_1 = 0^\circ$:



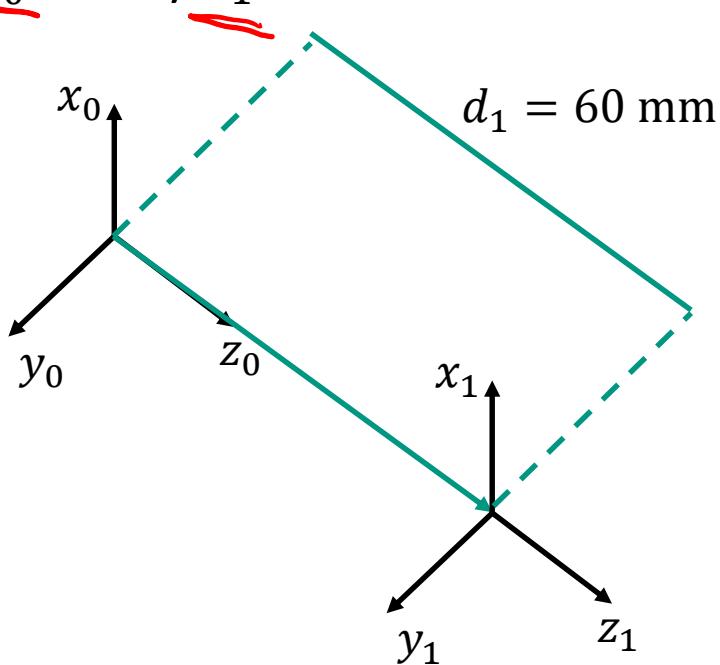
Exercise 2.1 (i): DH Transformation

- DH parameters: $\theta_1 = 0^\circ$, $d_1 = 60$ mm, $a_1 = 0$ mm, $\alpha_1 = 180^\circ$
- Rotation around z_0 -axis by $\theta_1 = 0^\circ$:



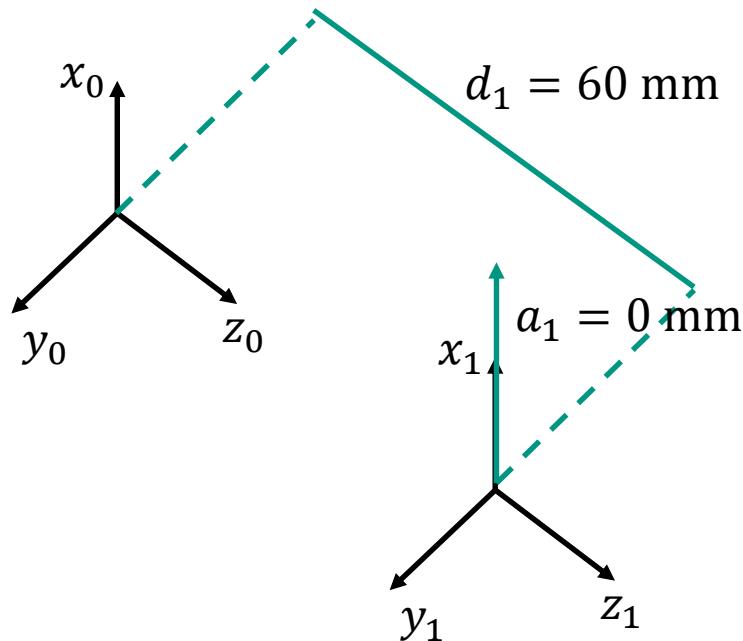
Exercise 2.1 (i): DH Transformation

- DH parameters: $\theta_1 = 0^\circ$, $d_1 = 60 \text{ mm}$, $a_1 = 0 \text{ mm}$, $\alpha_1 = 180^\circ$
- Translation along z_0 -axis by $d_1 = 60 \text{ mm}$:



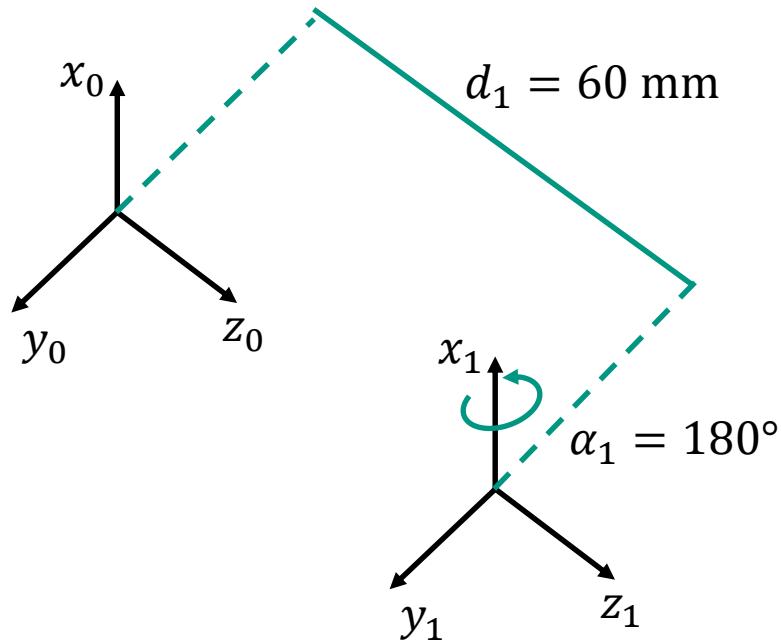
Exercise 2.1 (i): DH Transformation

- DH parameters: $\theta_1 = 0^\circ$, $d_1 = 60 \text{ mm}$, $a_1 = 0 \text{ mm}$, $\alpha_1 = 180^\circ$
- Translation along x_1 -axis by $a_1 = 0 \text{ mm}$:



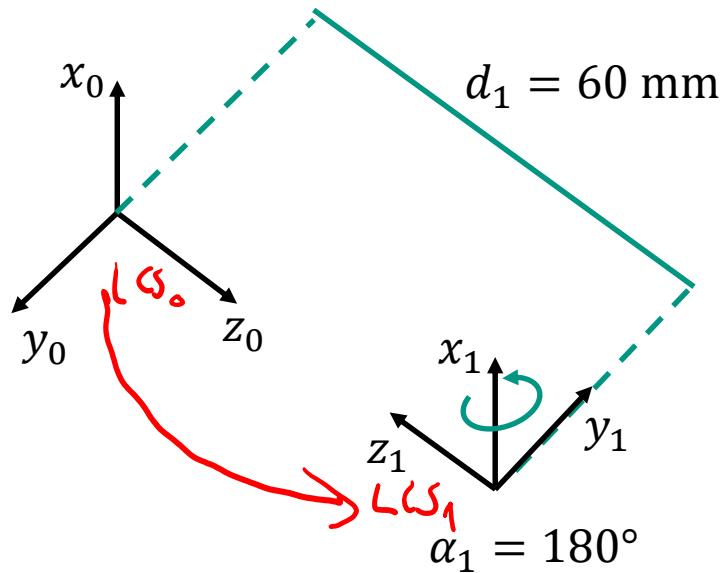
Exercise 2.1 (i): DH Transformation

- DH parameters: $\theta_1 = 0^\circ, d_1 = 60 \text{ mm}, a_1 = 0 \text{ mm}, \alpha_1 = 180^\circ$
- Rotation around x_1 -axis by $\alpha_1 = 180^\circ$:



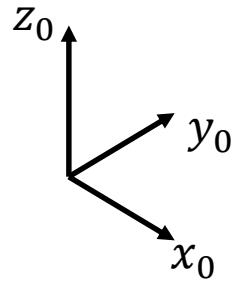
Exercise 2.1 (i): DH Transformation

- DH parameters: $\theta_1 = 0^\circ, d_1 = 60 \text{ mm}, a_1 = 0 \text{ mm}, \alpha_1 = 180^\circ$
- Rotation around x_1 -axis by $\alpha_1 = 180^\circ$:



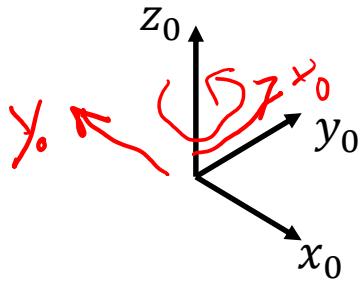
Exercise 2.1 (ii): DH Transformation

- DH parameters: $\theta_1 = 90^\circ, d_1 = -30 \text{ mm}, a_1 = 60 \text{ mm}, \alpha_1 = -90^\circ$



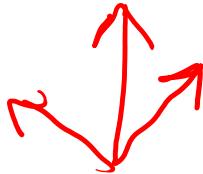
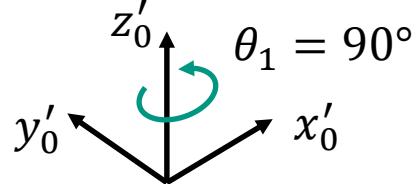
Exercise 2.1 (ii): DH Transformation

- DH parameters: $\theta_1 = 90^\circ$, $d_1 = -30$ mm, $a_1 = 60$ mm, $\alpha_1 = -90^\circ$
- Rotation around z_0 -axis by $\theta_1 = 90^\circ$:



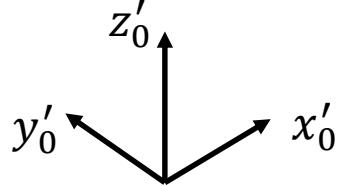
Exercise 2.1 (ii): DH Transformation

- DH parameters: $\theta_1 = 90^\circ$, $d_1 = -30$ mm, $a_1 = 60$ mm, $\alpha_1 = -90^\circ$
- Rotation around z_0 -axis by $\theta_1 = 90^\circ$:



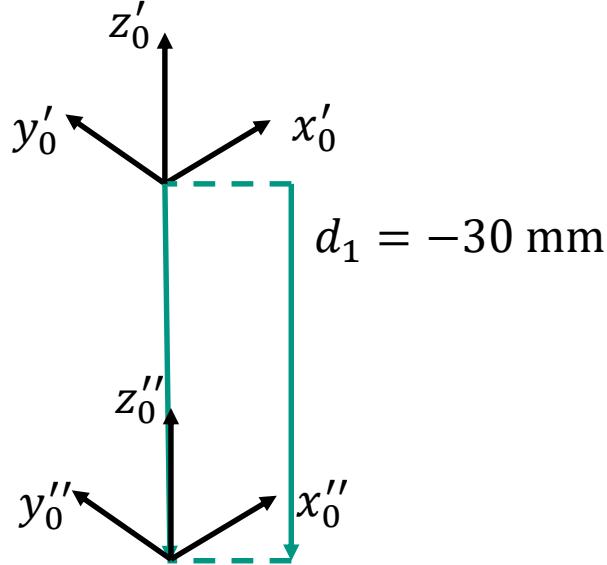
Exercise 2.1 (ii): DH Transformation

- DH parameters: $\theta_1 = 90^\circ$, $d_1 = -30 \text{ mm}$, $a_1 = 60 \text{ mm}$, $\alpha_1 = -90^\circ$
- Translation along z_0 -axis by $d_1 = -30 \text{ mm}$:



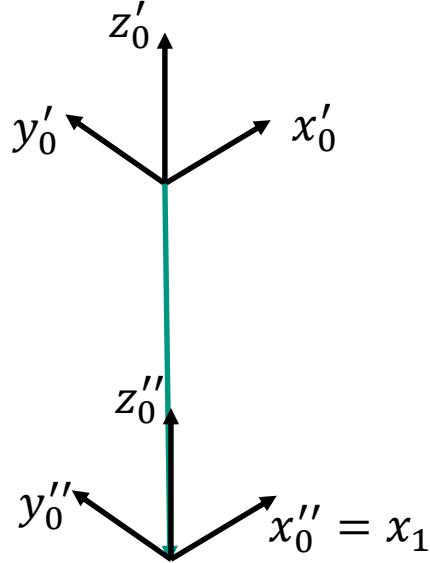
Exercise 2.1 (ii): DH Transformation

- DH parameters: $\theta_1 = 90^\circ$, $d_1 = -30 \text{ mm}$, $a_1 = 60 \text{ mm}$, $\alpha_1 = -90^\circ$
- Translation along z_0 -axis by $d_1 = -30 \text{ mm}$:



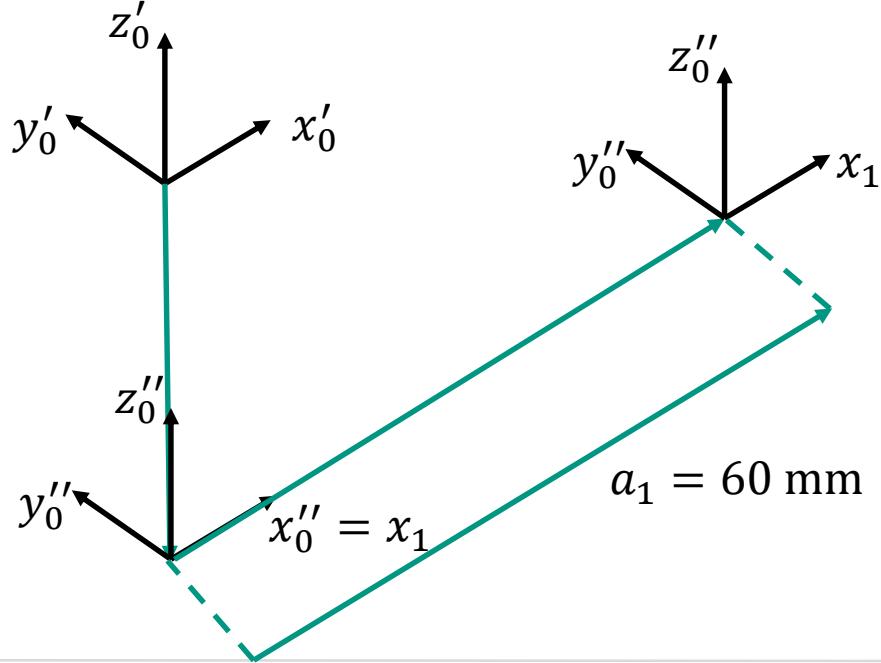
Exercise 2.1 (ii): DH Transformation

- DH parameters: $\theta_1 = 90^\circ$, $d_1 = -30$ mm, $a_1 = 60$ mm, $\alpha_1 = -90^\circ$
- Translation along x_1 -axis by $a_1 = 60$ mm:



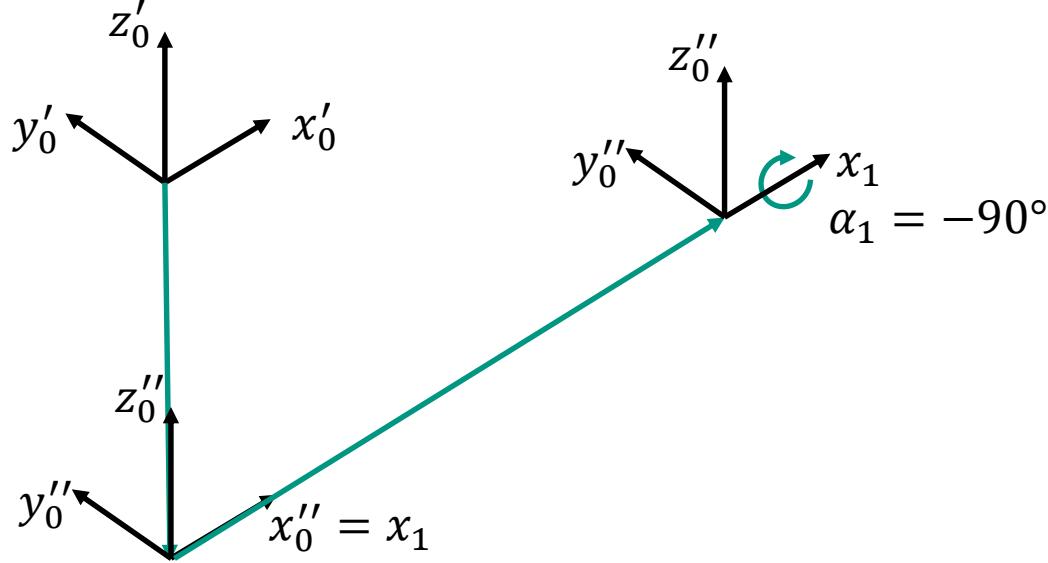
Exercise 2.1 (ii): DH Transformation

- DH parameters: $\theta_1 = 90^\circ$, $d_1 = -30 \text{ mm}$, $a_1 = 60 \text{ mm}$, $\alpha_1 = -90^\circ$
- Translation along x_1 -axis by $a_1 = 60 \text{ mm}$:



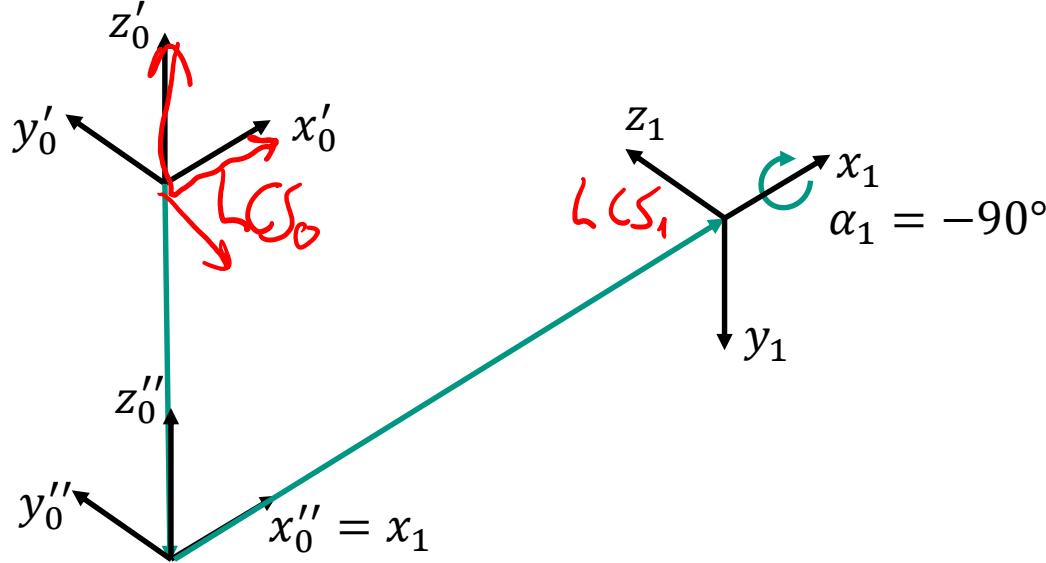
Exercise 2.1 (ii): DH Transformation

- DH parameters: $\theta_1 = 90^\circ$, $d_1 = -30$ mm, $a_1 = 60$ mm, $\alpha_1 = -90^\circ$
- Rotation around x_1 -axis by $\alpha_1 = -90^\circ$:



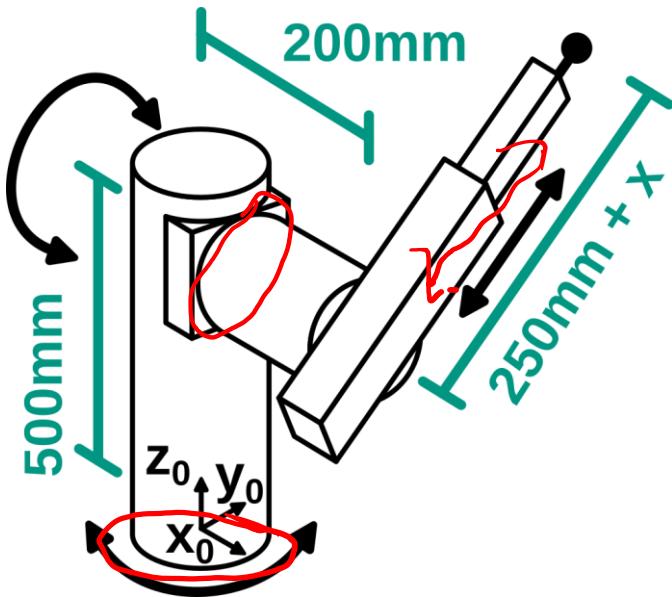
Exercise 2.1 (ii): DH Transformation

- DH parameters: $\theta_1 = 90^\circ$, $d_1 = -30$ mm, $a_1 = 60$ mm, $\alpha_1 = -90^\circ$
- Rotation around x_1 -axis by $\alpha_1 = -90^\circ$:



Exercise 2.2: DH Parameters

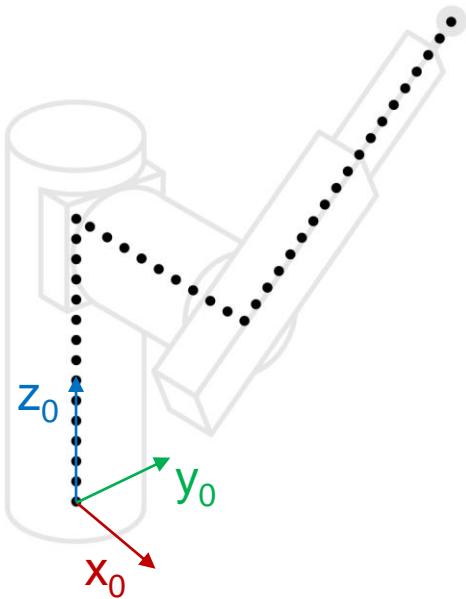
- Determine the DH parameters



Summary: Determination of the DH Parameters

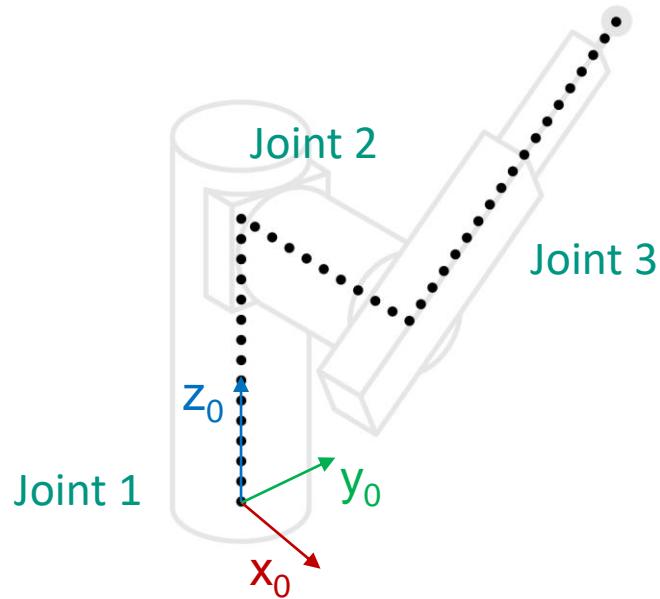
1. Sketch of the manipulator
2. Identify and enumerate the joints (1, ..., last link = n)
3. Draw the axes z_{i-1} for each joint i
4. Determine the parameters a_i between z_{i-1} and z_i
5. Draw the x_i -axes
6. Determine the parameters α_i (twist around the x_i -axes)
7. Determine the parameters d_i (link offset)
8. Determine the angles θ_i around the z_{i-1} -axes
9. Compose the joint transformation matrices $A_{i-1,i}$

Exercise 2.2: DH Parameters



- 1. Sketch of the manipulator**
2. Identify and enumerate the joints (1, ..., last link = n)
3. Draw the axes z_{i-1} for each joint i
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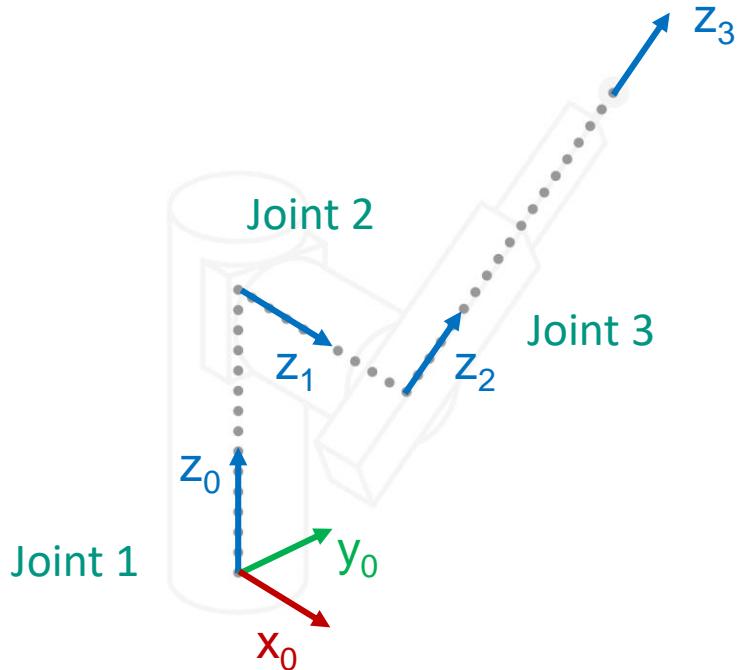
Exercise 2.2: DH Parameters



1. Sketch of the manipulator
2. Identify and enumerate the joints (1, ..., last link = n)
3. Draw the axes z_{i-1} for each joint i
4. Determine the parameters a_i between z_{i-1} and z_i
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9. Compose the joint transformation matrices $A_{i-1,i}$

Exercise 2.2: DH Parameters

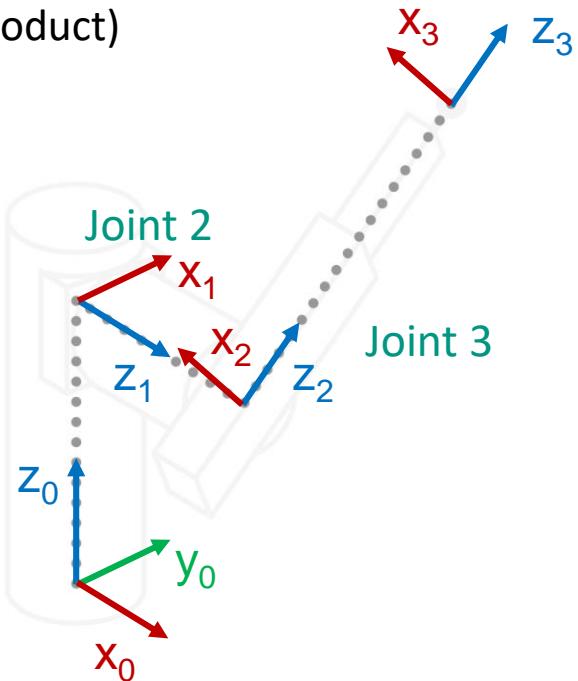
z_i runs along the **joint axis $i + 1$**



1. **Sketch** of the manipulator
2. Identify and **enumerate** the **joints** (1, ..., last link = n)
3. Draw the **axes z_{i-1}** for **each joint i**
4. Determine the parameters a_i between z_{i-1} and z_i
5. Draw the x_i -axes
6. Determine the parameters α_i (twist around the x_i -axes)
7. Determine the parameters d_i (link offset)
8. Determine the angles θ_i around the z_{i-1} -axes
9. Compose the **joint transformation matrices $A_{i-1,i}$**

Exercise 2.2: DH Parameters

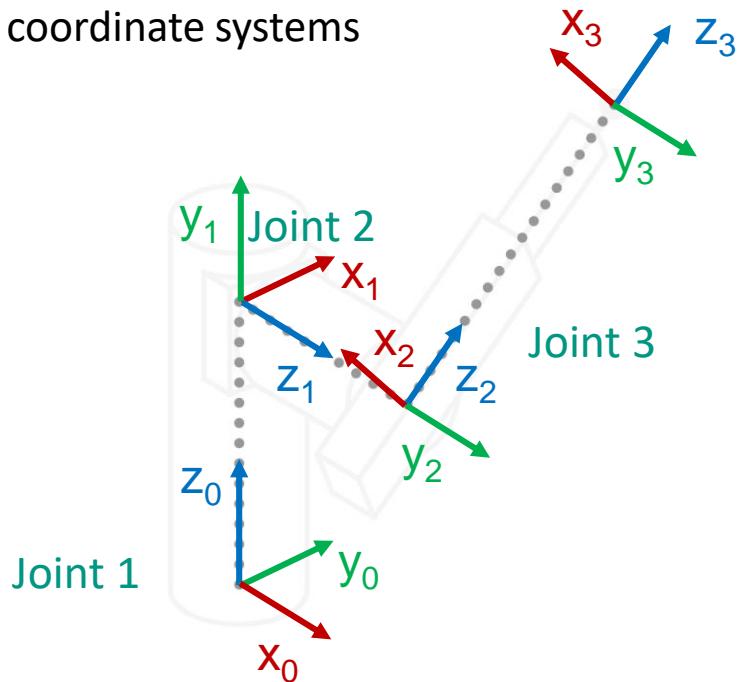
x_i lies along the **normal of z_{i-1} and z_i**
 (cross product)



1. Sketch of the manipulator
2. Identify and enumerate the joints (1, ..., last link = n)
3. Draw the axes z_{i-1} for each joint i
4. Determine the parameters a_i between z_{i-1} and z_i
5. Draw the x_i -axes
6. Determine the parameters α_i (twist around the x_i -axes)
7. Determine the parameters d_i (link offset)
8. Determine the angles θ_i around the z_{i-1} -axes
9. Compose the joint transformation matrices $A_{i-1,i}$

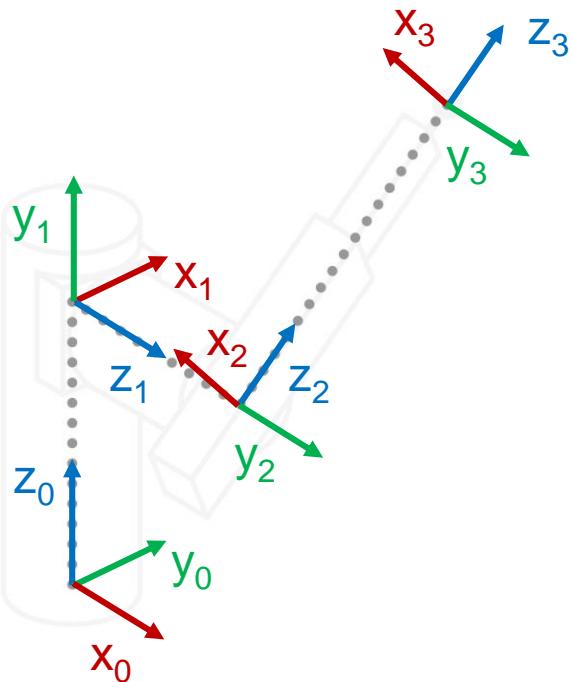
Exercise 2.2: DH Parameters

y_i to get right-handed orthonormal coordinate systems



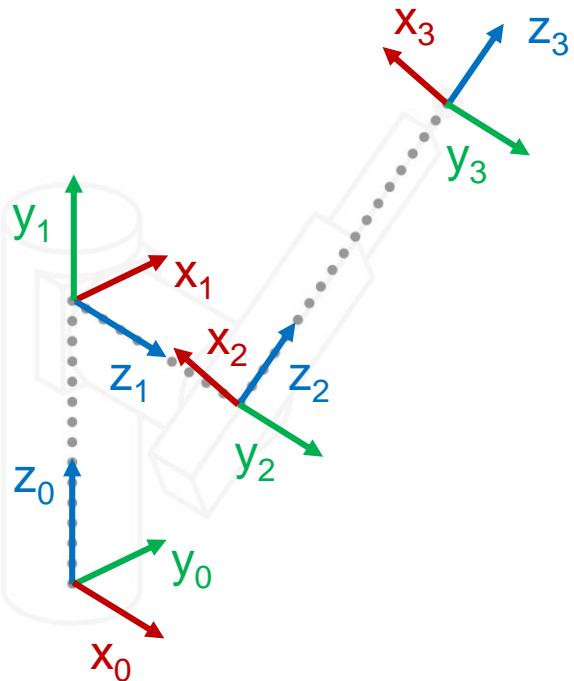
1. Sketch of the manipulator
2. Identify and enumerate the joints (1, ..., last link = n)
3. Draw the axes z_{i-1} for each joint i
4. Determine the parameters a_i between z_{i-1} and z_i
5. Draw the x_i -axes
6. Determine the parameters α_i (twist around the x_i -axes)
7. Determine the parameters d_i (link offset)
8. Determine the angles θ_i around the z_{i-1} -axes
9. Compose the joint transformation matrices $A_{i-1,i}$

Exercise 2.2: DH Parameters



1. Sketch of the manipulator
2. Identify and enumerate the joints ($1, \dots$, last link = n)
3. Draw the axes z_{i-1} for each joint i
4. Determine the parameters a_i between z_{i-1} and z_i
5. Draw the x_i -axes
6. Determine the parameters α_i (twist around the x_i -axes)
7. Determine the parameters d_i (link offset)
8. Determine the angles θ_i around the z_{i-1} -axes
9. Compose the joint transformation matrices $A_{i-1,i}$

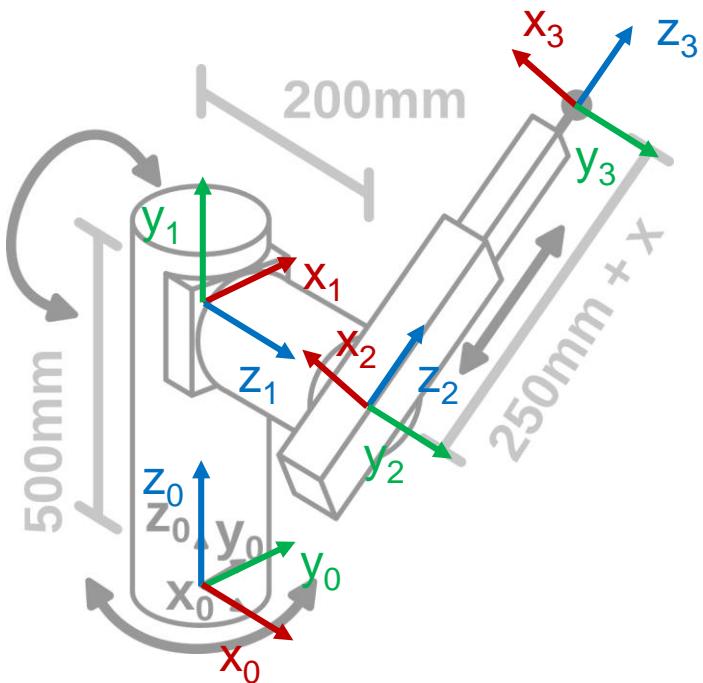
Exercise 2.2: DH Parameters



Joint angle θ_i is the angle from x_{i-1} to x_i around z_{i-1}

	θ	d	a	α
Joint 1	$90^\circ + \theta_1$			
Joint 2	$90^\circ + \theta_2$			
Joint 3	0°			

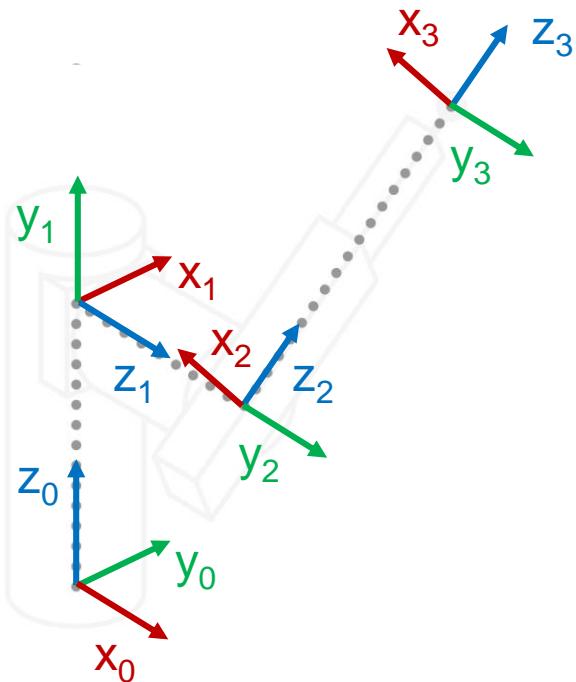
Exercise 2.2: DH Parameters



Link offset d_i is the distance between x_{i-1} -axis and x_i -axis **along the z_{i-1} -axis**

	θ	d	a	α
Joint 1	$90^\circ + \theta_1$	500 mm		
Joint 2	$90^\circ + \theta_2$	200 mm		
Joint 3	0°	250 mm + x		

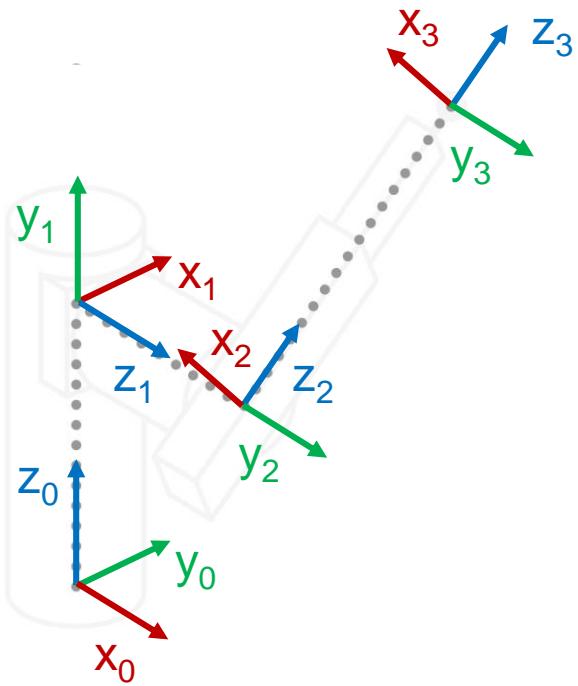
Exercise 2.2: DH Parameters



Link length a_i of an arm element i describes the **distance** from z_{i-1} to z_i along x_i

	θ	d	a	α
Joint 1	$90^\circ + \theta_1$	500 mm	0 mm	
Joint 2	$90^\circ + \theta_2$	200 mm	0 mm	
Joint 3	0°	250 mm + x	0 mm	

Exercise 2.2: DH Parameters



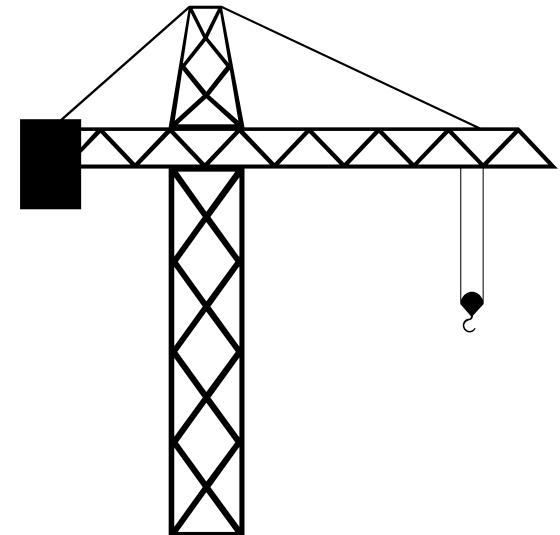
Link twist α_i describes the angle from z_{i-1} to z_i around x_i

	θ	d	a	α
Joint 1	$90^\circ + \theta_1$	500 mm	0 mm	90°
Joint 2	$90^\circ + \theta_2$	200 mm	0 mm	90°
Joint 3	0°	250 mm + x	0 mm	0°

Exercise 3: Crane

The crane can rotate by 360° and has a height of 20 m between ground and crane boom. The crane boom is 15 m long. The trolley stops 2 m away from the rotation axis. The hook can be lowered until reading the ground.

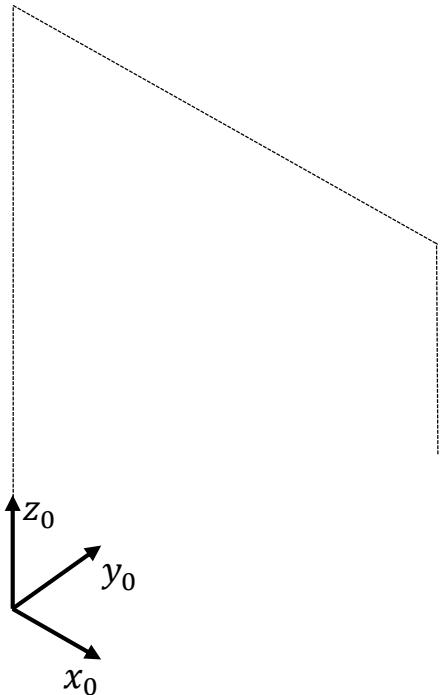
1. Determine the DH parameters of the crane and the resulting transformation matrix of the end effector.
2. Determine the Jacobian matrix of the end effector.
3. Determine the end effector velocities.



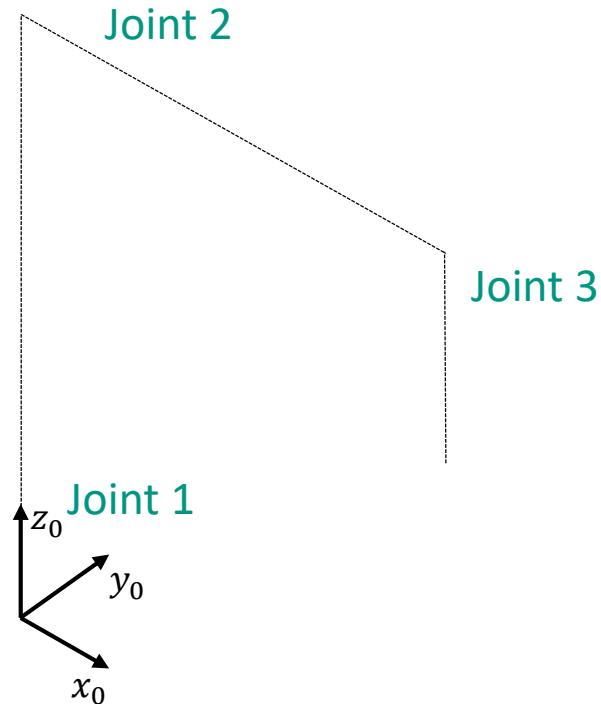
<https://thenounproject.com/term/crane/2225/>

mirrored (CC Attribution 3.0)

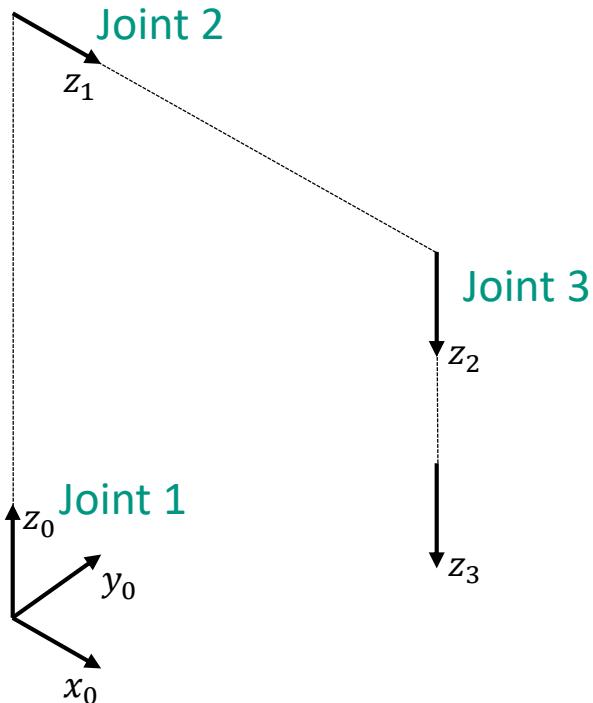
Exercise 3.1: DH Parameters of the Crane



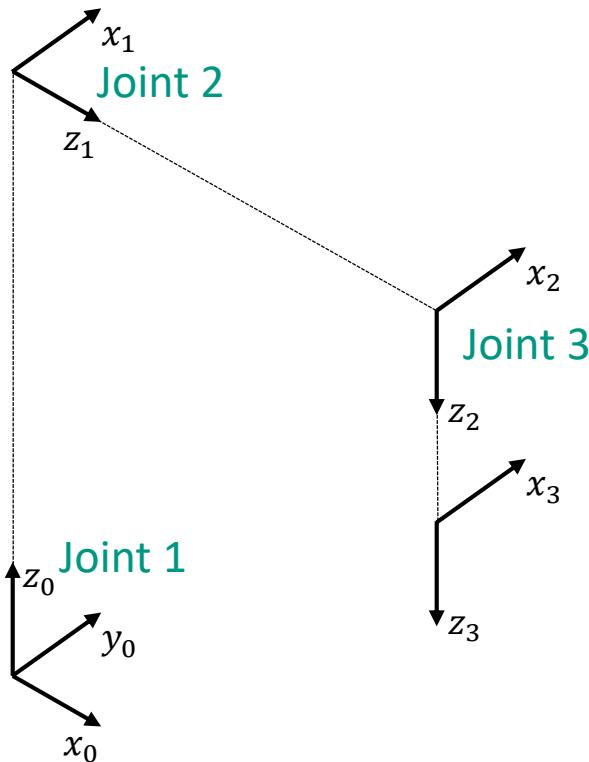
Exercise 3.1: DH Parameters of the Crane



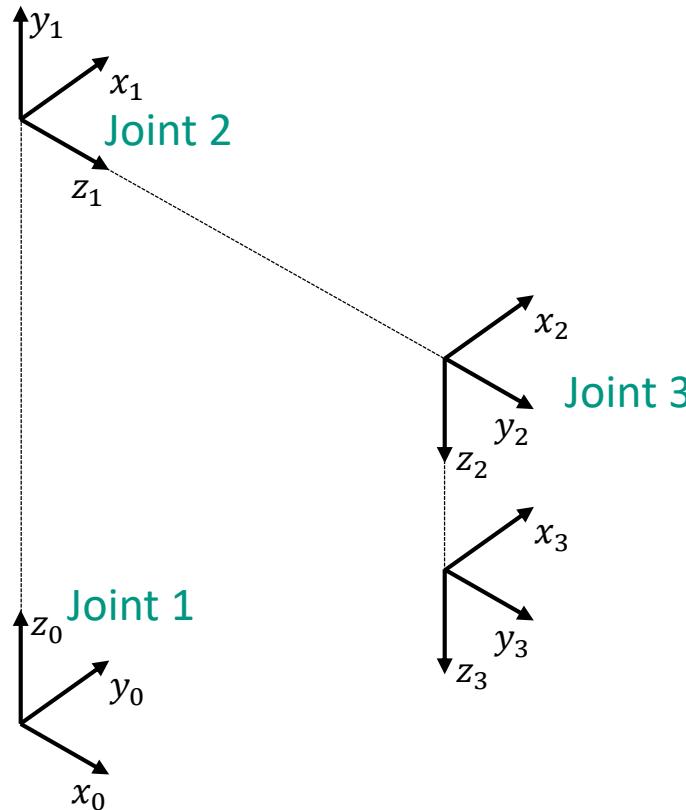
Exercise 3.1: DH Parameters of the Crane



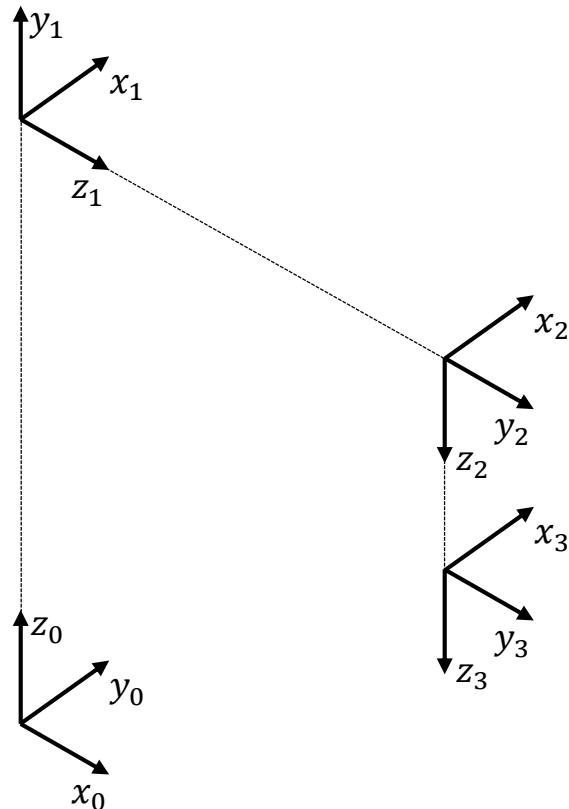
Exercise 3.1: DH Parameters of the Crane



Exercise 3.1: DH Parameters of the Crane

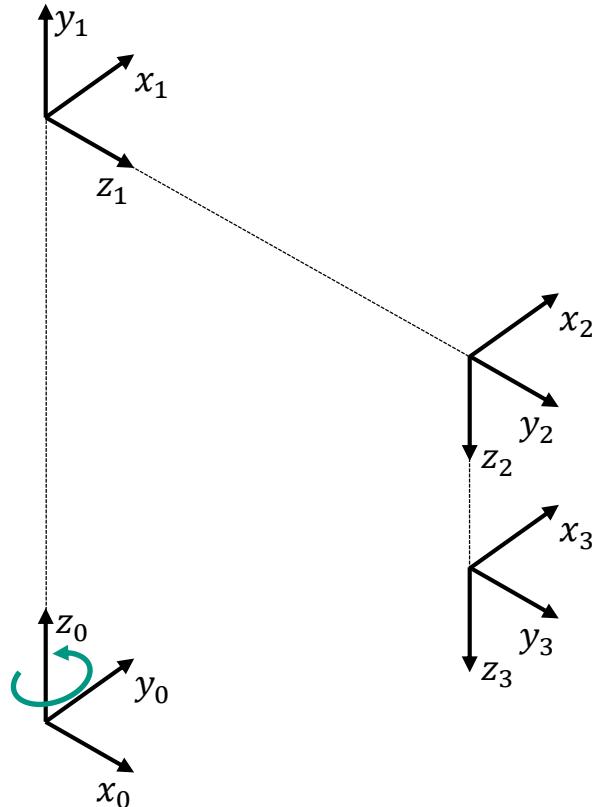


Exercise 3.1: DH Parameters of the Crane



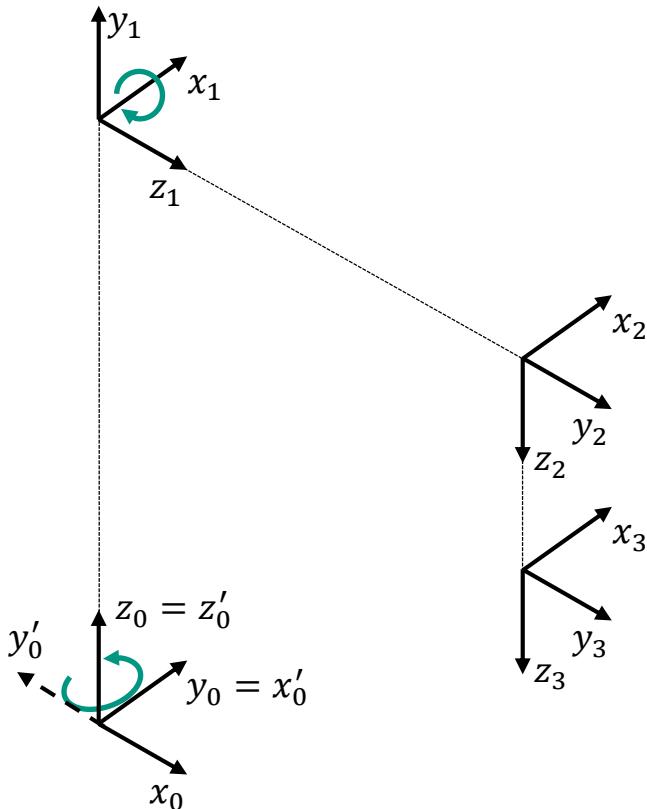
	θ	d	a	α
Joint 1				
Joint 2				
Joint 3				

Exercise 3.1: DH Parameters of the Crane



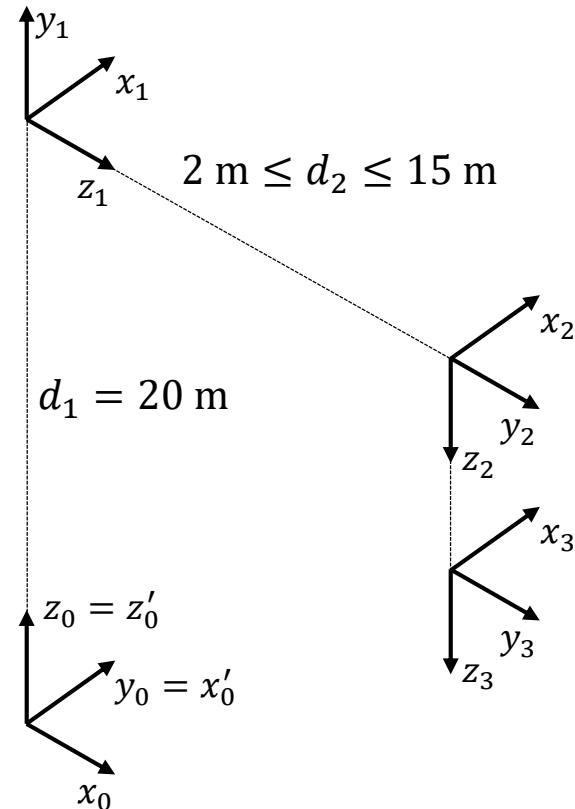
	θ	d	a	α
Joint 1	$\theta_1 + 90^\circ$	20 m		
Joint 2				
Joint 3				

Exercise 3.1: DH Parameters of the Crane



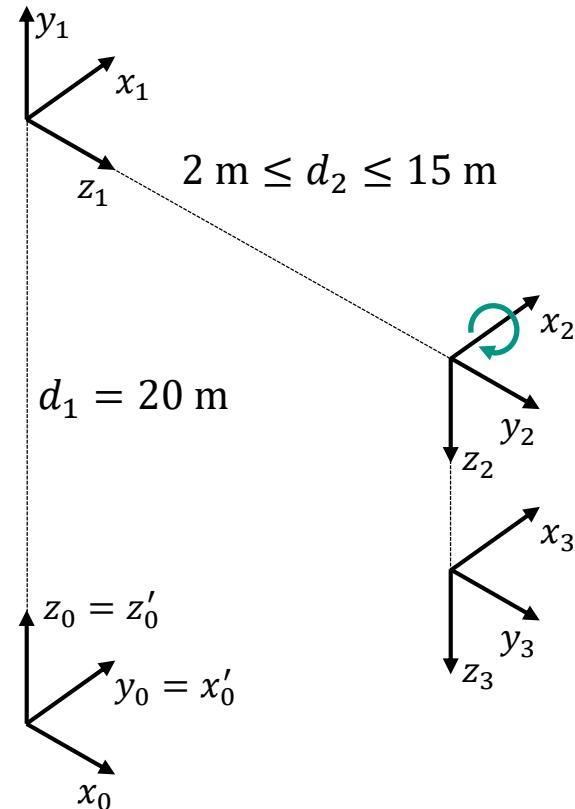
	θ	d	a	α
Joint 1	$\theta_1 + 90^\circ$	20 m	0 m	90°
Joint 2				
Joint 3				

Exercise 3.1: DH Parameters of the Crane



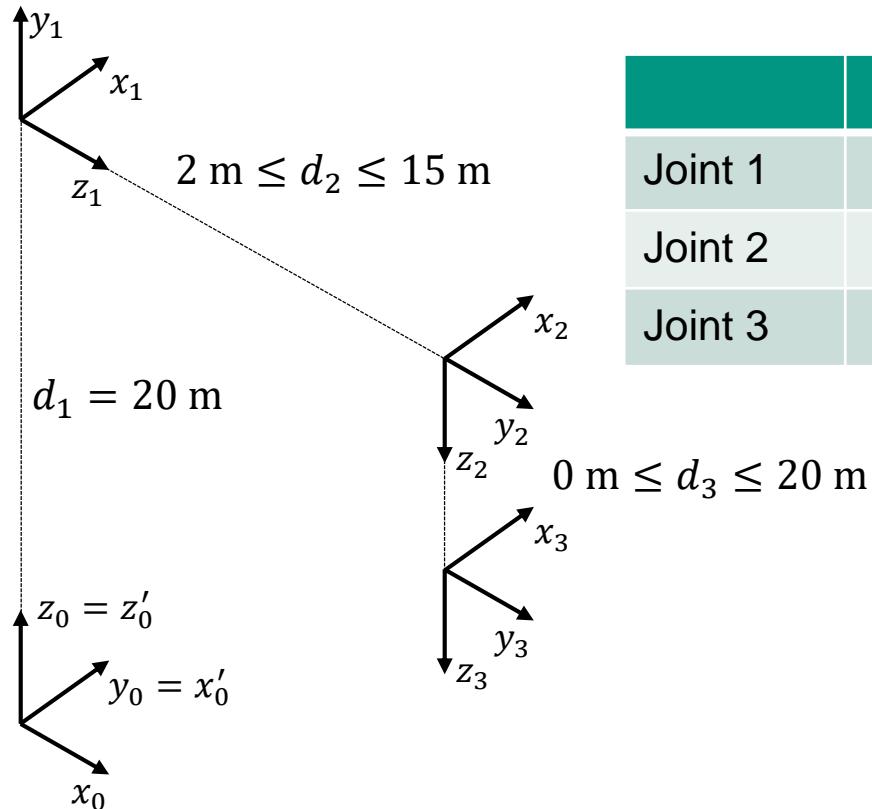
	θ	d	a	α
Joint 1	$\theta_1 + 90^\circ$	20 m	0 m	90°
Joint 2	0°	$2 \text{ m} \leq d_2 \leq 15 \text{ m}$		
Joint 3				

Exercise 3.1: DH Parameters of the Crane



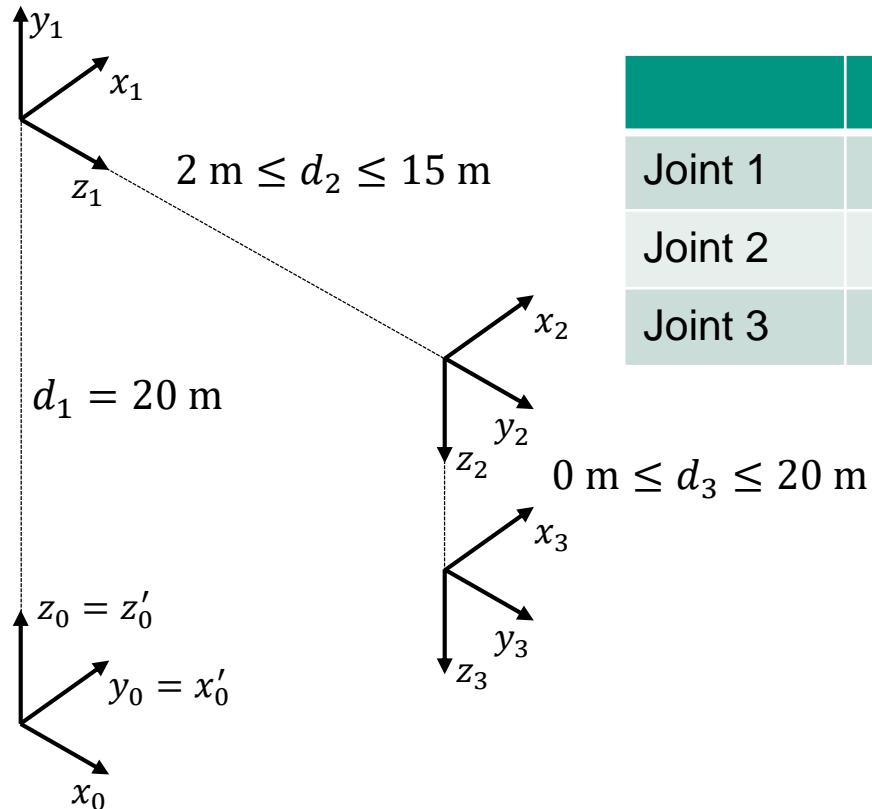
	θ	d	a	α
Joint 1	$\theta_1 + 90^\circ$	20 m	0 m	90°
Joint 2	0°	$2 \text{ m} \leq d_2 \leq 15 \text{ m}$	0 m	90°
Joint 3				

Exercise 3.1: DH Parameters of the Crane



	θ	d	a	α
Joint 1	$\theta_1 + 90^\circ$	20 m	0 m	90°
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Exercise 3.1: DH Parameters of the Crane



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Joint 1	$\theta_1 + 90^\circ$	20 m	0 m	90°
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Joint 3	0°	$0 \text{ m} \leq d_3 \leq 20 \text{ m}$	0 m	0°

Exercise 3.1: Transformation Matrix of the Crane

	θ	d	a	α
Joint 1	$\theta_1 + 90^\circ$	20 m	0 m	90°
Joint 2	0°	$2 \text{ m} \leq d_2 \leq 15 \text{ m}$	0 m	90°
Joint 3	0°	$0 \text{ m} \leq d_3 \leq 20 \text{ m}$	0 m	0°

DH Transformation Matrices

- Transformation from LCS_{i-1} to LCS_i

$$A_{i-1,i} = R_{z_{i-1}}(\theta_i) \cdot T_{z_{i-1}}(d_i) \cdot T_{x_i}(a_i) \cdot R_{x_i}(\alpha_i) =$$

$$= \begin{bmatrix} \cos \theta_i & -\sin \theta_i \cdot \cos \alpha_i & \sin \theta_i \cdot \sin \alpha_i & a_i \cdot \cos \theta_i \\ \sin \theta_i & \cos \theta_i \cdot \cos \alpha_i & -\cos \theta_i \cdot \sin \alpha_i & a_i \cdot \sin \theta_i \\ 0 & \sin \alpha_i & \cos \alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Exercise 3.1: Transformation Matrix of the Crane

	θ	d	a	α
Joint 1	$\theta_1 + 90^\circ$	20 m	0 m	90°
Joint 2	0°	$2 \text{ m} \leq d_2 \leq 15 \text{ m}$	0 m	90°
Joint 3	0°	$0 \text{ m} \leq d_3 \leq 20 \text{ m}$	0 m	0°

$$T_{0,1} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) & 0 \\ \sin(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) & 0 \\ 0 & 1 & 0 & 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

Exercise 3.1: Transformation Matrix of the Crane

	θ	d	a	α
Joint 1	$\theta_1 + 90^\circ$	20 m	0 m	90°
Joint 2	0°	$2 \text{ m} \leq d_2 \leq 15 \text{ m}$	0 m	90°
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$$T_{0,1} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) & 0 \\ \sin(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) & 0 \\ 0 & 1 & 0 & 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$T_{1,2} = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

Exercise 3.1: Transformation Matrix of the Crane

	θ	d	a	α
Joint 1	$\theta_1 + 90^\circ$	20 m	0 m	90°
Joint 2	0°	$2 \text{ m} \leq d_2 \leq 15 \text{ m}$	0 m	90°
Joint 3	0°	$0 \text{ m} \leq d_3 \leq 20 \text{ m}$	0 m	0°

$$T_{0,1} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) & 0 \\ \sin(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) & 0 \\ 0 & 1 & 0 & 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$T_{1,2} = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 1 & 0 & d_2 \\ 0 & 0 & 0 & 1 \end{pmatrix} \quad T_{2,3} = \begin{pmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & d_3 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

Exercise 3.1: Transformation Matrix of the Crane

$$T_{0,3} = T_{0,1} \cdot T_{1,2} \cdot T_{2,3}$$

Exercise 3.1: Transformation Matrix of the Crane

$$T_{0,3} = T_{0,1} \cdot T_{1,2} \cdot T_{2,3}$$

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Exercise 3.1: Transformation Matrix of the Crane

$$T_{0,3} = T_{0,1} \cdot T_{1,2} \cdot T_{2,3}$$

$$= \begin{pmatrix} \cos(\theta_1 + 90^\circ) & \sin(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) d_2 \\ \sin(\theta_1 + 90^\circ) & -\cos(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) d_2 \\ 0 & 0 & -1 & 20 \\ 0 & 0 & 0 & 1 \end{pmatrix} \cdot T_{2,3}$$

$$= \begin{pmatrix} \cos(\theta_1 + 90^\circ) & \sin(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) d_2 \\ \sin(\theta_1 + 90^\circ) & -\cos(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) d_2 \\ 0 & 0 & -1 & -d_3 + 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$T_{0,3} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & \sin(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) d_2 \\ \sin(\theta_1 + 90^\circ) & -\cos(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) d_2 \\ 0 & 0 & -1 & -d_3 + 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

- Determine the Jacobian matrix J .

Exercise 3.2: Jacobian Matrix of the End Effector

$$T_{0,3} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & \sin(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) d_2 \\ \sin(\theta_1 + 90^\circ) & -\cos(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) d_2 \\ 0 & 0 & -1 & -d_3 + 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

- Determine the Jacobian matrix J .
- Each column of the Jacobian matrix corresponds to a joint θ_i of the kinematic chain

$$J = \begin{pmatrix} \frac{\partial f}{\partial \theta_1} & \dots & \frac{\partial f}{\partial \theta_n} \end{pmatrix} \in \mathbb{R}^{6 \times n}$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$T_{0,3} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & \sin(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) d_2 \\ \sin(\theta_1 + 90^\circ) & -\cos(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) d_2 \\ 0 & 0 & -1 & -d_3 + 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

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$$J = \begin{pmatrix} \frac{\partial f}{\partial \theta_1} & \dots & \frac{\partial f}{\partial \theta_n} \end{pmatrix} \in \mathbb{R}^{6 \times n}$$

$$J = \begin{pmatrix} \frac{\partial f}{\partial \theta_1} & \frac{\partial f}{\partial d_2} & \frac{\partial f}{\partial d_3} \end{pmatrix} \in \mathbb{R}^{6 \times 3}$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$f(\theta_1, d_2, d_3) = (x, y, z, \alpha, \beta, \gamma)^T$$

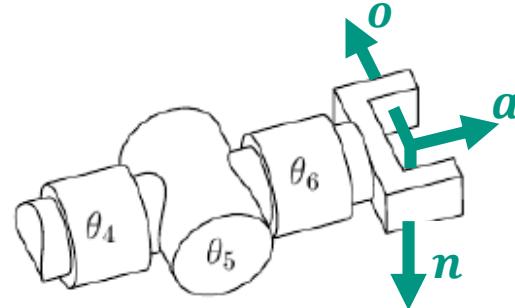
$$T_{0,3} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & \sin(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) d_2 \\ \sin(\theta_1 + 90^\circ) & -\cos(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) d_2 \\ 0 & 0 & -1 & -d_3 + 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

RPY Euler Angles

$$R_s = R_z(\gamma) \cdot R_y(\beta) \cdot R_x(\alpha)$$

$$\begin{aligned} \cos x &= cx \\ \sin x &= sx \end{aligned}$$

a: approach
n: normal
o: orientation



$$\begin{pmatrix} n_x & o_x & a_x \\ n_y & o_y & a_y \\ n_z & o_z & a_z \end{pmatrix} == \begin{pmatrix} c\gamma & -s\gamma & 0 \\ s\gamma & c\gamma & 0 \\ 0 & 0 & 1 \end{pmatrix} \cdot \begin{pmatrix} c\beta & 0 & s\beta \\ 0 & 1 & 0 \\ -s\beta & 0 & c\beta \end{pmatrix} \cdot \begin{pmatrix} 1 & 0 & 0 \\ 0 & c\alpha & -s\alpha \\ 0 & s\alpha & c\alpha \end{pmatrix}$$

$$\begin{pmatrix} n_x & o_x & a_x \\ n_y & o_y & a_y \\ n_z & o_z & a_z \end{pmatrix} = \begin{pmatrix} c\beta \cdot c\gamma & s\alpha \cdot s\beta \cdot c\gamma - c\alpha \cdot s\gamma & s\alpha \cdot s\gamma + c\alpha \cdot s\beta \cdot c\gamma \\ c\beta \cdot s\gamma & s\alpha \cdot s\beta \cdot s\gamma + c\alpha \cdot c\gamma & c\alpha \cdot s\beta \cdot s\gamma - s\alpha \cdot c\gamma \\ -s\beta & s\alpha \cdot c\beta & c\alpha \cdot c\beta \end{pmatrix}$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$f(\theta_1, d_2, d_3) = (x, y, z, \alpha, \beta, \gamma)^T$$

$$T_{0,3} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & \sin(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) d_2 \\ \sin(\theta_1 + 90^\circ) & -\cos(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) d_2 \\ 0 & 0 & -1 & -d_3 + 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$x = \sin(\theta_1 + 90^\circ) d_2$$

$$y = -\cos(\theta_1 + 90^\circ) d_2$$

$$z = -d_3 + 20$$

$$\beta = \text{asin}(-n_z) = \text{asin}(0) = 0$$

$$\begin{pmatrix} n_x & o_x & a_x \\ n_y & o_y & a_y \\ \textcolor{red}{n_z} & o_z & a_z \end{pmatrix} =$$

$$\begin{pmatrix} c\beta \cdot cy & s\alpha \cdot s\beta \cdot cy - c\alpha \cdot sy & s\alpha \cdot sy + c\alpha \cdot s\beta \cdot cy \\ c\beta \cdot sy & s\alpha \cdot s\beta \cdot sy + c\alpha \cdot cy & c\alpha \cdot s\beta \cdot sy - s\alpha \cdot cy \\ -s\beta & s\alpha \cdot c\beta & c\alpha \cdot c\beta \end{pmatrix}$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$f(\theta_1, d_2, d_3) = (x, y, z, \alpha, \beta, \gamma)^T$$

$$T_{0,3} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & \sin(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) d_2 \\ \sin(\theta_1 + 90^\circ) & -\cos(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) d_2 \\ 0 & 0 & -1 & -d_3 + 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$x = \sin(\theta_1 + 90^\circ) d_2$$

$$y = -\cos(\theta_1 + 90^\circ) d_2$$

$$z = -d_3 + 20$$

$$\beta = \text{asin}(-n_z) = \text{asin}(0) = 0$$

$$\cos \beta \sin \alpha = 0, \cos \beta \cos \alpha = -1$$

$$\Rightarrow \alpha = \pi$$

$$\begin{pmatrix} n_x & o_x & a_x \\ n_y & o_y & a_y \\ n_z & o_z & a_z \end{pmatrix} =$$

$$\begin{pmatrix} c\beta \cdot c\gamma & s\alpha \cdot s\beta \cdot c\gamma - c\alpha \cdot s\gamma & s\alpha \cdot s\gamma + c\alpha \cdot s\beta \cdot c\gamma \\ c\beta \cdot s\gamma & s\alpha \cdot s\beta \cdot s\gamma + c\alpha \cdot c\gamma & c\alpha \cdot s\beta \cdot s\gamma - s\alpha \cdot c\gamma \\ -s\beta & s\alpha \cdot c\beta & c\alpha \cdot c\beta \end{pmatrix}$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$f(\theta_1, d_2, d_3) = (x, y, z, \alpha, \beta, \gamma)^T$$

$$T_{0,3} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & \sin(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) d_2 \\ \sin(\theta_1 + 90^\circ) & -\cos(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) d_2 \\ 0 & 0 & -1 & -d_3 + 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$x = \sin(\theta_1 + 90^\circ) d_2$$

$$y = -\cos(\theta_1 + 90^\circ) d_2$$

$$z = -d_3 + 20$$

$$\beta = \text{asin}(-n_z) = \text{asin}(0) = 0$$

$$\cos \beta \sin \alpha = 0, \cos \beta \cos \alpha = -1$$

$$\Rightarrow \alpha = \pi$$

$$\gamma = \text{atan} \left(\frac{n_y}{n_x} \right) = \text{atan} \left(\frac{\sin(\theta_1 + 90^\circ)}{\cos(\theta_1 + 90^\circ)} \right)$$

$$\begin{pmatrix} n_x & o_x & a_x \\ n_y & o_y & a_y \\ n_z & o_z & a_z \end{pmatrix} =$$

$$\begin{pmatrix} c\beta \cdot c\gamma & s\alpha \cdot s\beta \cdot c\gamma - c\alpha \cdot s\gamma & s\alpha \cdot s\gamma + c\alpha \cdot s\beta \cdot c\gamma \\ c\beta \cdot s\gamma & s\alpha \cdot s\beta \cdot s\gamma + c\alpha \cdot c\gamma & c\alpha \cdot s\beta \cdot s\gamma - s\alpha \cdot c\gamma \\ -s\beta & s\alpha \cdot c\beta & c\alpha \cdot c\beta \end{pmatrix}$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$f(\theta_1, d_2, d_3) = (x, y, z, \alpha, \beta, \gamma)^T$$

$$T_{0,3} = \begin{pmatrix} \cos(\theta_1 + 90^\circ) & \sin(\theta_1 + 90^\circ) & 0 & \sin(\theta_1 + 90^\circ) d_2 \\ \sin(\theta_1 + 90^\circ) & -\cos(\theta_1 + 90^\circ) & 0 & -\cos(\theta_1 + 90^\circ) d_2 \\ 0 & 0 & -1 & -d_3 + 20 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$x = \sin(\theta_1 + 90^\circ) d_2$$

$$y = -\cos(\theta_1 + 90^\circ) d_2$$

$$z = -d_3 + 20$$

$$\beta = \text{asin}(-n_z) = \text{asin}(0) = 0$$

$$\cos \beta \sin \alpha = 0, \cos \beta \cos \alpha = -1$$

$$\Rightarrow \alpha = \pi$$

$$\gamma = \text{atan} \left(\frac{n_y}{n_x} \right) = \text{atan} \left(\frac{\sin(\theta_1 + 90^\circ)}{\cos(\theta_1 + 90^\circ)} \right) = \text{atan}(\tan(\theta_1 + 90^\circ)) = \theta_1 + 90^\circ$$

$$\begin{pmatrix} n_x & o_x & a_x \\ n_y & o_y & a_y \\ n_z & o_z & a_z \end{pmatrix} = \begin{pmatrix} c\beta \cdot c\gamma & s\alpha \cdot s\beta \cdot c\gamma - c\alpha \cdot s\gamma & s\alpha \cdot s\gamma + c\alpha \cdot s\beta \cdot c\gamma \\ c\beta \cdot s\gamma & s\alpha \cdot s\beta \cdot s\gamma + c\alpha \cdot c\gamma & c\alpha \cdot s\beta \cdot s\gamma - s\alpha \cdot c\gamma \\ -s\beta & s\alpha \cdot c\beta & c\alpha \cdot c\beta \end{pmatrix}$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$f(\theta_1, d_2, d_3) = (x, y, z, \alpha, \beta, \gamma)^T$$

$$x = \sin(\theta_1 + 90^\circ) d_2$$

$$y = -\cos(\theta_1 + 90^\circ) d_2$$

$$z = -d_3 + 20$$

$$\alpha = \pi$$

$$\beta = 0$$

$$\gamma = \theta_1 + 90^\circ$$

$$J = \begin{pmatrix} \frac{\partial f}{\partial \theta_1} & \frac{\partial f}{\partial d_2} & \frac{\partial f}{\partial d_3} \end{pmatrix} \in \mathbb{R}^{6 \times 3}$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$f(\theta_1, d_2, d_3) = (x, y, z, \alpha, \beta, \gamma)^T$$

$$x = \sin(\theta_1 + 90^\circ) d_2$$

$$y = -\cos(\theta_1 + 90^\circ) d_2$$

$$z = -d_3 + 20$$

$$\alpha = \pi$$

$$\beta = 0$$

$$\gamma = \theta_1 + 90^\circ$$

$$J = \begin{pmatrix} \frac{\partial f}{\partial \theta_1} & \frac{\partial f}{\partial d_2} & \frac{\partial f}{\partial d_3} \end{pmatrix} \in \mathbb{R}^{6 \times 3}$$

$$\frac{\partial f}{\partial \theta_1} = \left(\frac{\partial x}{\partial \theta_1}, \frac{\partial y}{\partial \theta_1}, \frac{\partial z}{\partial \theta_1}, \frac{\partial \alpha}{\partial \theta_1}, \frac{\partial \beta}{\partial \theta_1}, \frac{\partial \gamma}{\partial \theta_1} \right)^T$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$\frac{\partial}{\partial \theta_1}(x) = \frac{\partial}{\partial \theta_1} (\sin(\theta_1 + 90^\circ) d_2)$$

$$\frac{\partial}{\partial \theta_1}(y) = \frac{\partial}{\partial \theta_1} (-\cos(\theta_1 + 90^\circ) d_2)$$

$$\frac{\partial}{\partial \theta_1}(z) = \frac{\partial}{\partial \theta_1} (-d_3 + 20)$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$\begin{aligned}\frac{\partial}{\partial \theta_1}(x) &= \frac{\partial}{\partial \theta_1}(\sin(\theta_1 + 90^\circ) d_2) \\ &= \cos(\theta_1 + 90^\circ) d_2\end{aligned}$$

$$\begin{aligned}\frac{\partial}{\partial \theta_1}(y) &= \frac{\partial}{\partial \theta_1}(-\cos(\theta_1 + 90^\circ) d_2) \\ &= \sin(\theta_1 + 90^\circ) d_2\end{aligned}$$

$$\frac{\partial}{\partial \theta_1}(z) = \frac{\partial}{\partial \theta_1}(-d_3 + 20) = 0$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$\frac{\partial}{\partial \theta_1}(\alpha) = \frac{\partial}{\partial \theta_1}(\pi)$$

$$\frac{\partial}{\partial \theta_1}(\beta) = \frac{\partial}{\partial \theta_1}(0)$$

$$\frac{\partial}{\partial \theta_1}(\gamma) = \frac{\partial}{\partial \theta_1}(\theta_1 + 90^\circ)$$

$$\frac{\partial f}{\partial \theta_1} =$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$\frac{\partial}{\partial \theta_1}(\alpha) = \frac{\partial}{\partial \theta_1}(\pi) = 0$$

$$\frac{\partial}{\partial \theta_1}(\beta) = \frac{\partial}{\partial \theta_1}(0) = 0$$

$$\frac{\partial}{\partial \theta_1}(\gamma) = \frac{\partial}{\partial \theta_1}(\theta_1 + 90^\circ) = 1$$

$$\frac{\partial f}{\partial \theta_1} = (\cos(\theta_1 + 90^\circ) d_2, \sin(\theta_1 + 90^\circ) d_2, 0, 0, 0, 1)^T$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$\frac{\partial}{\partial d_2}(x) = \frac{\partial}{\partial d_2}(\sin(\theta_1 + 90^\circ) d_2)$$

$$\frac{\partial}{\partial d_2}(y) = \frac{\partial}{\partial d_2}(-\cos(\theta_1 + 90^\circ) d_2)$$

$$\frac{\partial}{\partial d_2}(z) = \frac{\partial}{\partial d_2}(\alpha) = \frac{\partial}{\partial d_2}(\beta) = \frac{\partial}{\partial d_2}(\gamma)$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$\begin{aligned}\frac{\partial}{\partial d_2}(x) &= \frac{\partial}{\partial d_2}(\sin(\theta_1 + 90^\circ) d_2) \\ &= \sin(\theta_1 + 90^\circ)\end{aligned}$$

$$\begin{aligned}\frac{\partial}{\partial d_2}(y) &= \frac{\partial}{\partial d_2}(-\cos(\theta_1 + 90^\circ) d_2) \\ &= -\cos(\theta_1 + 90^\circ)\end{aligned}$$

$$\frac{\partial}{\partial d_2}(z) = \frac{\partial}{\partial d_2}(\alpha) = \frac{\partial}{\partial d_2}(\beta) = \frac{\partial}{\partial d_2}(\gamma) = 0$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$\frac{\partial}{\partial d_3}(z) = \frac{\partial}{\partial d_3}(-d_3 + 20)$$

$$\frac{\partial}{\partial d_3}(x) = \frac{\partial}{\partial d_3}(y) = \frac{\partial}{\partial d_3}(\alpha) = \frac{\partial}{\partial d_3}(\beta) = \frac{\partial}{\partial d_3}(\gamma)$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$\begin{aligned}\frac{\partial}{\partial d_3}(z) &= \frac{\partial}{\partial d_3}(-d_3 + 20) \\ &= -1\end{aligned}$$

$$\frac{\partial}{\partial d_3}(x) = \frac{\partial}{\partial d_3}(y) = \frac{\partial}{\partial d_3}(\alpha) = \frac{\partial}{\partial d_3}(\beta) = \frac{\partial}{\partial d_3}(\gamma) = 0$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$J = \begin{pmatrix} \frac{\partial f}{\partial \theta_1} & \frac{\partial f}{\partial d_2} & \frac{\partial f}{\partial d_3} \end{pmatrix} \in \mathbb{R}^{6 \times 3}$$

Exercise 3.2: Jacobian Matrix of the End Effector

$$J = \begin{pmatrix} \frac{\partial f}{\partial \theta_1} & \frac{\partial f}{\partial d_2} & \frac{\partial f}{\partial d_3} \end{pmatrix} \in \mathbb{R}^{6 \times 3}$$

$$J = \begin{pmatrix} \cos(\theta_1 + 90^\circ) d_2 & \sin(\theta_1 + 90^\circ) & 0 \\ \sin(\theta_1 + 90^\circ) d_2 & -\cos(\theta_1 + 90^\circ) & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (1,1)

- Determine the end effector velocity resulting from the following combination of the crane configuration q and the joint velocity p .

$$q_1 = (90, 10, 10)^T, p_1 = (1, 1, 1)^T$$

Exercise 3.3: Velocity of the End Effector (1,1)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_1 = (90, 10, 10)^T, \mathbf{p}_1 = (1, 1, 1)^T$$

$$\mathbf{v}_1 = J(\mathbf{q}_1) \cdot \mathbf{p}_1$$

Exercise 3.3: Velocity of the End Effector (1,1)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_1 = (90, 10, 10)^T, \mathbf{p}_1 = (1, 1, 1)^T$$

$$\mathbf{v}_1 = J(\mathbf{q}_1) \cdot \mathbf{p}_1$$

$$\mathbf{v}_1 = \begin{pmatrix} \cos(\theta_1 + 90^\circ) \cdot d_2 & \sin(\theta_1 + 90^\circ) & 0 \\ \sin(\theta_1 + 90^\circ) \cdot d_2 & -\cos(\theta_1 + 90^\circ) & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (1,1)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_1 = (90, 10, 10)^T, \mathbf{p}_1 = (1, 1, 1)^T$$

$$\mathbf{v}_1 = J(\mathbf{q}_1) \cdot \mathbf{p}_1$$

$$\mathbf{v}_1 = \begin{pmatrix} \cos(90^\circ + 90^\circ) \cdot 10 & \sin(90^\circ + 90^\circ) & 0 \\ \sin(90^\circ + 90^\circ) \cdot 10 & -\cos(90^\circ + 90^\circ) & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (1,1)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_1 = (90, 10, 10)^T, \mathbf{p}_1 = (1, 1, 1)^T$$

$$\mathbf{v}_1 = J(\mathbf{q}_1) \cdot \mathbf{p}_1$$

$$\mathbf{v}_1 = \begin{pmatrix} -10 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (1,1)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_1 = (90, 10, 10)^T, \mathbf{p}_1 = (1, 1, 1)^T$$

$$\mathbf{v}_1 = J(\mathbf{q}_1) \cdot \mathbf{p}_1$$

$$\mathbf{v}_1 = \begin{pmatrix} -10 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} 1 \\ 1 \\ 1 \end{pmatrix} = \begin{pmatrix} -10 \\ 1 \\ -1 \\ 0 \\ 0 \\ 1 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (1,2)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_1 = (90, 10, 10)^T, \mathbf{p}_2 = (-1, -1, 0)^T$$

$$\mathbf{v}_2 = J(\mathbf{q}_1) \cdot \mathbf{p}_2$$

Exercise 3.3: Velocity of the End Effector (1,2)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_1 = (90, 10, 10)^T, \mathbf{p}_2 = (-1, -1, 0)^T$$

$$\mathbf{v}_2 = J(\mathbf{q}_1) \cdot \mathbf{p}_2$$

$$\mathbf{v}_2 = \begin{pmatrix} -10 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} -1 \\ -1 \\ 0 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (1,2)

- Determine the end effector velocity resulting from the following combination of the crane configuration q and the joint velocity p .

$$q_1 = (90, 10, 10)^T, p_2 = (-1, -1, 0)^T$$

$$v_2 = J(q_1) \cdot p_2$$

$$v_2 = \begin{pmatrix} -10 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} -1 \\ -1 \\ 0 \end{pmatrix} = \begin{pmatrix} 10 \\ -1 \\ 0 \\ 0 \\ 0 \\ -1 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (2,2)

- Determine the end effector velocity resulting from the following combination of the crane configuration q and the joint velocity p .

$$q_2 = (180, 2, 15)^T, p_2 = (-1, -1, 0)$$

$$v_3 = J(q_2) \cdot p_2$$

Exercise 3.3: Velocity of the End Effector (2,2)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_2 = (180, 2, 15)^T, \mathbf{p}_2 = (-1, -1, 0)$$

$$\mathbf{v}_3 = J(\mathbf{q}_2) \cdot \mathbf{p}_2$$

$$\mathbf{v}_3 = \begin{pmatrix} \cos(\theta_1 + 90^\circ) \cdot d_2 & \sin(\theta_1 + 90^\circ) & 0 \\ \sin(\theta_1 + 90^\circ) \cdot d_2 & -\cos(\theta_1 + 90^\circ) & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} -1 \\ -1 \\ 0 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (2,2)

- Determine the end effector velocity resulting from the following combination of the crane configuration q and the joint velocity p .

$$q_2 = (180, 2, 15)^T, p_2 = (-1, -1, 0)$$

$$v_3 = J(q_2) \cdot p_2$$

$$v_3 = \begin{pmatrix} \cos(180^\circ + 90^\circ) \cdot 2 & \sin(180^\circ + 90^\circ) & 0 \\ \sin(180^\circ + 90^\circ) \cdot 2 & -\cos(180^\circ + 90^\circ) & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} -1 \\ -1 \\ 0 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (2,2)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_2 = (\textcolor{red}{180}, \textcolor{blue}{2}, 15)^T, \mathbf{p}_2 = (-1, -1, 0)$$

$$\mathbf{v}_3 = J(\mathbf{q}_2) \cdot \mathbf{p}_2$$

$$\mathbf{v}_3 = \begin{pmatrix} 0 & -1 & 0 \\ -2 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} -1 \\ -1 \\ 0 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (2,2)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_2 = (\textcolor{red}{180}, \textcolor{blue}{2}, 15)^T, \mathbf{p}_2 = (-1, -1, 0)$$

$$\mathbf{v}_3 = J(\mathbf{q}_2) \cdot \mathbf{p}_2$$

$$\mathbf{v}_3 = \begin{pmatrix} 0 & -1 & 0 \\ -2 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} -1 \\ -1 \\ 0 \end{pmatrix} = \begin{pmatrix} 1 \\ 2 \\ 0 \\ 0 \\ 0 \\ -1 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (2,3)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_2 = (180, 2, 15)^T, \mathbf{p}_3 = (2, -1, 2)$$

$$\mathbf{v}_4 = J(\mathbf{q}_2) \cdot \mathbf{p}_3$$

Exercise 3.3: Velocity of the End Effector (2,3)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_2 = (180, 2, 15)^T, \mathbf{p}_3 = (2, -1, 2)$$

$$\mathbf{v}_4 = J(\mathbf{q}_2) \cdot \mathbf{p}_3$$

$$\mathbf{v}_4 = \begin{pmatrix} 0 & -1 & 0 \\ -2 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} 2 \\ -1 \\ 2 \end{pmatrix}$$

Exercise 3.3: Velocity of the End Effector (2,3)

- Determine the end effector velocity resulting from the following combination of the crane configuration \mathbf{q} and the joint velocity \mathbf{p} .

$$\mathbf{q}_2 = (180, 2, 15)^T, \mathbf{p}_3 = (2, -1, 2)$$

$$\mathbf{v}_4 = J(\mathbf{q}_2) \cdot \mathbf{p}_3$$

$$\mathbf{v}_4 = \begin{pmatrix} 0 & -1 & 0 \\ -2 & 0 & 0 \\ 0 & 0 & -1 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 0 & 0 \end{pmatrix} \cdot \begin{pmatrix} 2 \\ -1 \\ 2 \end{pmatrix} = \begin{pmatrix} 1 \\ -4 \\ -2 \\ 0 \\ 0 \\ 2 \end{pmatrix}$$